



# CERTIFICATE

By Authority Of  
THE UNITED STATES OF AMERICA  
Legally Binding Document

By the Authority Vested By Part 5 of the United States Code § 552(a) and Part 1 of the Code of Regulations § 51 the attached document has been duly INCORPORATED BY REFERENCE and shall be considered legally binding upon all citizens and residents of the United States of America. *HEED THIS NOTICE:* Criminal penalties may apply for noncompliance.



**Document Name:** ASME B31G: Manual for Determining the Remaining Strength of Corroded Pipelines

**CFR Section(s):** 49 CFR 192.485(c)

**Standards Body:** American Society of Mechanical Engineers



*Official Incorporator:*

THE EXECUTIVE DIRECTOR  
OFFICE OF THE FEDERAL REGISTER  
WASHINGTON, D.C.



ASME Code for Pressure Piping, B31  
An American National Standard

**REAFFIRMED 2004**

FOR CURRENT COMMITTEE PERSONNEL  
PLEASE E-MAIL [CS@asme.org](mailto:CS@asme.org)

**ASME B31G-1991**

(REVISION OF ANSI/ASME B31G-1984)

**Manual for Determining  
the Remaining Strength  
of Corroded Pipelines**

**A Supplement to ASME B31 Code  
for Pressure Piping**

AN AMERICAN NATIONAL STANDARD

ASME CODE FOR PRESSURE PIPING, B31

# **Manual for Determining the Remaining Strength of Corroded Pipelines**

**A Supplement to ASME B31 Code  
for Pressure Piping**

**ASME B31G-1991**  
(REVISION OF ANSI/ASME B31G-1984)



The American Society of  
Mechanical Engineers

345 East 47th Street, New York, N.Y. 10017 —



Date of Issuance: June 27, 1991

The 1991 edition of this Manual will be revised when public comment or Committee actions necessitate the issuance of a new edition, or it will be reviewed and reaffirmed 5 years from the date of approval of this edition. No addenda service is provided with this publication. Written interpretations of the requirements of this Manual will not be issued to the current edition.

ASME is the registered trademark of The American Society of Mechanical Engineers.

This code or standard was developed under procedures accredited as meeting the criteria for American National Standards. The Consensus Committee that approved the code or standard was balanced to assure that individuals from competent and concerned interests have had an opportunity to participate. The proposed code or standard was made available for public review and comment which provides an opportunity for additional public input from industry, academia, regulatory agencies, and the public-at-large.

ASME does not "approve," "rate," or "endorse" any item, construction, proprietary device, or activity.

ASME does not take any position with respect to the validity of any patent rights asserted in connection with any items mentioned in this document, and does not undertake to insure anyone utilizing a standard against liability for infringement of any applicable Letters Patent, nor assume any such liability. Users of a code or standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, is entirely their own responsibility.

Participation by federal agency representative(s) or person(s) affiliated with industry is not to be interpreted as government or industry endorsement of this code or standard.

ASME accepts responsibility for only those interpretations issued in accordance with governing ASME procedures and policies which preclude the issuance of interpretations by individual volunteers.

No part of this document may be reproduced in any form,  
in an electronic retrieval system or otherwise,  
without the prior written permission of the publisher.

Copyright © 1991 by  
THE AMERICAN SOCIETY OF MECHANICAL ENGINEERS  
All Rights Reserved  
Printed in the U.S.A.



## FOREWORD

(This Foreword is not a part of ASME B31G-1991.)

It is recognized by pipeline companies that some sections of high pressure pipelines, particularly those installed a number of years ago, have experienced some corrosion. Where corrosion is found, pipeline operators have been deeply concerned about the need for a method of determining the remaining strength of these corroded areas. If the corrosion does not penetrate the pipe wall, what is the pressure containing capability of the remaining pipe metal in terms of its ability to continue to operate safely at the maximum allowable operating pressure (MAOP) of the pipeline system? Thus, one of the needs of the pipeline industry has been a procedure that will help operators, particularly field personnel, make decisions on existing pipelines, when exposed for any purpose, as to whether any corroded region may be left in service or whether it needs to be repaired or replaced. Such determinations must be based upon sound research and extensive testing in order to provide safe and conservative guidelines on which to base field decisions. The Manual provides procedures to assist in this determination.

Parts 2, 3, and 4 are based on Appendices G-6, G-7, and G-8 of the ASME Guide for Gas Transmission and Distribution Piping Systems, 1983 Edition. They are included in this Manual for use by field operators to determine the remaining strength of corroded pipe. The technology is based on research done in the Columbus laboratories of the Battelle Memorial Institute; specifically, their report *Summary of Research to Determine the Strength of Corroded Areas in Line Pipe*, July 10, 1971.

A revision to the 1984 edition of the Manual was undertaken in 1989. The revision includes a number of clarifications and corrections. The computer program presented in Appendix B and used to produce a printed table of maximum acceptable corrosion lengths for a given pipe diameter, and up to ten wall thicknesses of that diameter, was upgraded.

This Manual was approved by ASME and subsequently by the American National Standards Institute on May 20, 1991.



## ASME CODE FOR PRESSURE PIPING, B31

### OFFICERS

**R. E. Feigel, *Chairman***  
**L. E. Hayden, Jr., *Vice Chairman***  
**C. J. Gomez, *Secretary***

### COMMITTEE PERSONNEL

**P. A. Bourquin, Wolff & Munier International, Hawthorne, New York**  
**A. J. Breugelmans, Lvndhurst, New Jersey**  
**J. D. Byers, Mobil Research & Development, Princeton, New Jersey**  
**J. J. Chappell, Anchor/Darling Valve Co., Williamsport, Pennsylvania**  
**L. F. Clynch, CONOCO Mid-Continental Division, Ponca City, Oklahoma**  
**P. C. DuPernell, Lancaster, New York**  
**R. E. Feigel, Hartford Steam Boiler Inspection and Insurance Co., Hartford, Connecticut**  
**D. M. Fischer, Sargent & Lundy, Chicago, Illinois**  
**P. D. Flenner, Consumers Power Co., Jackson, Michigan**  
**P. H. Gardner, Hercules Inc., Wilmington, Delaware**  
**R. W. Haupt, Pressure Piping Engrg Associates Inc., Foster City, California**  
**L. E. Hayden, Jr., Victaulic Company of America, Easton, Pennsylvania**  
**R. R. Hoffmann, Federal Energy Regulatory Commission, Washington, DC**  
**B. P. Holbrook, Riley Stoker Corp., Worcester, Massachusetts**  
**H. M. Howarth, Trenton, New Jersey**  
**W. B. McGehee, Spring, Texas**  
**A. J. Shoup, Sr., Houston, Texas**  
**G. W. Spohn, III, Dixie Constructors, Inc., Gaffney, South Carolina**  
**H. A. Sosnin, Jenkintown, Pennsylvania**  
**D. H. Wade, Texas Utilities Electric Co., Dallas, Texas**

### B31.8 GAS TRANSMISSION AND DISTRIBUTION PIPING SYSTEMS SECTION COMMITTEE

**A. J. Shoup, Sr., *Chairman*, Houston, Texas**  
**W. B. McGehee, *Vice Chairman*, Spring, Texas**  
**C. J. Gomez, *Secretary*, ASME, New York, New York**  
**W. C. Alexander, Shreveport, Louisiana**  
**R. J. T. Appleby, Exxon Co., USA Thousand Oaks, California**  
**J. E. Beech, Texas Gas Transmission Corp., Owensboro, Kentucky**  
**C. Boshuizen, T. D. Williamson Inc., Tulsa, Oklahoma**  
**L. E. Brooks, Delta Gulf Corp., Shreveport, Louisiana**  
**F. E. Buck, Grove Valve & Regulator Co., Oakland, California**  
**J. S. Chin, ANR Pipeline Co., Detroit, Michigan**  
**W. L. Clayton, Entex Inc., Houston, Texas**  
**P. J. Cory, Bowie, Maryland**



R. L. Dean, ConReg Associates, Bellaire, Texas  
 A. J. Del Buono, CMI-Princeton Inc., Princeton, Kentucky  
 P. W. Denning, Texas Gas Transmission Corp., Owensboro, Kentucky  
 M. J. Epperson, Texaco Inc., Bellaire, Texas  
 J. J. Fallon, Jr., Public Service Electric & Gas Co., Newark, New Jersey  
 F. R. Fleet, Natural Gas Pipeline Company of America, Lombard, Illinois  
 M. A. Francis, LTV Steel Tubular Products Co., Youngstown, Ohio  
 P. R. Goodholm, Visalia, California  
 J. E. Hansford, Enron Gas Pipeline Operating Co., Houston, Texas  
 D. J. Hicks, Endeco Engineering Consultants, Tulsa, Oklahoma  
 D. T. Hisey, ARCO Transportation Alaska, Anchorage, Alaska  
 M. C. Hocking, Transcontinental Gas Pipe Line, Houston, Texas  
 E. A. Jonas, Bethlehem, Pennsylvania  
 J. J. Kieffer, Union Carbide Corp., Tonawanda, New York  
 J. D. McNorgan, Southern California Gas Co., Los Angeles, California  
 A. I. Macdonald, Upland, California  
 R. E. Miller, Columbia Gas Systems Service Corp., Columbus, Ohio  
 R. A. Mueller, OXY USA Inc., Tulsa, Oklahoma  
 P. O. Mullens, Phillips Petroleum Co., Bartlesville, Oklahoma  
 D. L. Price, Texas Eastern Gas Pipe Line Co., Harrisburg, Pennsylvania  
 W. F. Quinn, El Paso Natural Gas Co., El Paso, Texas  
 A. T. Richardson, Tenneco Gas Transportation Co., Houston, Texas  
 C. G. Roberts, Williams Brothers Engineering Co., Tulsa, Oklahoma  
 R. A. Schmidt, Ladish Co., Russelville, Arkansas  
 B. Taksa, Gulf Interstate Engineering, Houston, Texas  
 C. J. Tateosian, Walnut Creek, California  
 A. T. Tyler, Gulf Interstate Engineering Co., Houston, Texas  
 H. M. Wilkinson, Houston, Texas  
 G. J. Wolf, Office of Pipeline Safety, U. S. Department of Transportation, Washington, District of  
 Columbia  
 R. A. Wolf, Transok Inc., Tulsa, Oklahoma  
 J. M. Wood, Oklahoma Natural Gas Co., Tulsa, Oklahoma  
 D. W. Wright, Sun Pipe Line Co., Tulsa, Oklahoma  
 C. C. Wright, Jr., Paola, Kansas  
 J. S. Zurcher, Panhandle Eastern Pipe Line Co., Houston, Texas

### **B31 COORDINATING COMMITTEE**

D. M. Fischer, *Chairman*, Sargent & Lundy, Chicago, Illinois  
 C. J. Gomez, *Secretary*, ASME, New York, New York  
 L. E. Hayden, Jr., Victaulic Company of America, Easton, Pennsylvania  
 R. R. Hoffmann, Federal Energy Regulatory Commission, Washington, District of Columbia  
 H. A. Sosnin, Jenkintown, Pennsylvania

### **B31 FABRICATION AND EXAMINATION TECHNICAL COMMITTEE**

P. D. Flenner, *Chairman*, Consumers Power Co., Jackson, Michigan  
 C. J. Gomez, *Secretary*, ASME, New York, New York  
 P. C. DuPernell, Lancaster, New York  
 T. E. Estilow, Newark, Delaware  
 L. E. Hartsell, Fluor Daniel, Dallas, Texas  
 D. G. Hopkins, E I duPont de Nemours & Co., Newark, Delaware  
 A. D. Nance, Evans, Georgia  
 R. I. Seals, Berkeley, California  
 H. A. Sosnin, Jenkintown, Pennsylvania





## B31 MECHANICAL DESIGN COMMITTEE

R. W. Haupt, *Chairman*, Pressure Piping Engrg Associates Inc., Foster City, California  
C. J. Gomez, *Secretary*, ASME, New York, New York  
J. P. Breen, O'Donnell & Associates Inc., Pittsburgh, Pennsylvania  
A. C. Dzykewicz, Bristol, Rhode Island  
J. A. Graziano, Farragut, Tennessee  
B. P. Holbrook, Riley Stoker Corp., Worcester, Massachusetts  
W. J. Koves, UOP Inc., Des Plaines, Illinois  
P. L. Lin, Fluor Engineers Inc., Chicago, Illinois  
T. Q. McCawley, Charlotte, North Carolina  
E. Michalopoulos, Hartford Steam Boiler Inspection and Insurance Co., Hartford, Connecticut  
J. C. Minichiello, ABB Impell Corp., Lincolnshire, Illinois  
A. D. Nance, Evans, Georgia  
T. W. Pickel, Jr., Martin Marietta Energy Systems Inc., Oak Ridge, Tennessee  
E. C. Reed, Babcock & Wilcox Co., Barberton, Ohio  
Q. N. Truong, Houston, Texas  
G. E. Woods, Kingwood, Texas

## B31 CONFERENCE GROUP

M. E. Bajandas, Department of Labor & Human Resources, Hato Ray, Puerto Rico  
R. Beaucamp, Department of Labor, Lincoln, Nebraska  
J. E. Brennan, Division of Boiler Inspection, Columbus, Ohio  
W. E. Brown, State of Kansas, Shawnee Mission, Kansas  
G. Bynog, Texas Department of Labor & Standards, Austin, Texas  
R. Coomes, Department of Housing, Buildings, and Construction, Frankfort, Kentucky  
Z. C. Cordero, Michigan Department of Labor, Lansing, Michigan  
J. C. Cvar, Division of Boiler Safety, Dover, Delaware  
A. W. Diamond, Department of Labour & Manpower, St. Johns, Newfoundland, Canada  
M. P. Fitzpatrick, Department of Labour & Human Resources, Fredericton, New Brunswick, Canada  
J. W. Greenawalt, Jr., Oklahoma Department of Labor, Oklahoma City, Oklahoma  
G. Grodecki, Ministry of Consumer & Commercial Relations, Toronto, Ontario, Canada  
R. D. Herman, Saskatchewan Labour, Regina, Saskatchewan, Canada  
D. W. Johansen, Public Service Commission, Jefferson City, Missouri  
A. Justin, State of Minnesota, Saint Paul, Minnesota  
J. T. Little, Industrial Commission of Arizona, Phoenix, Arizona  
W. T. Malloy, Washington Utilities & Transportation Commission, Olympia, Washington  
R. G. Marini, New Hampshire Public Utilities Commission, Concord, New Hampshire  
I. W. Mault, Labour & Manpower, Winnipeg, Manitoba, Canada  
A. W. Meiring, Department of Fire Prevention & Building Safety, Indianapolis, Indiana  
E. E. Morgan, Boiler Inspection Section, Denver, Colorado  
J. W. Morvant, Office of State Fire Marshal, Baton Rouge, Louisiana  
R. F. Mullaney, Boiler & Pressure Vessel Safety Branch, Vancouver, British Columbia, Canada  
W. A. Owen, North Dakota Public Service Commission, Bismarck, North Dakota  
W. M. Picardo, Department of Consumer & Regulatory Affairs, Washington, District of Columbia  
R. Sauve, Government of Quebec, Montreal, Quebec, Canada  
P. Sher, Department of Public Utility Control, New Britain, Connecticut  
H. E. Shutt, Illinois Commerce Commission, Springfield, Illinois  
J. L. Smith, Alberta Department of Labour, Edmonton, Alberta, Canada  
R. L. Smith, Public Service Commission, Columbia, South Carolina  
M. L. Snow, Jr., Department of Commerce and Insurance, Nashville, Tennessee  
E. L. Sparrow, Bureau of Pipeline Safety, Newark, New Jersey  
D. Stursma, Iowa State Commerce Commission, Des Moines, Iowa  
R. P. Sullivan, Department of Labor, Augusta, Maine  
C. W. Thompson, Department of Labor, Little Rock, Arkansas



R. W. Vindich, Department of Labor & Industry, Harrisburgh, Pennsylvania  
L. E. Waldrop, Public Service Commission, Montgomery, Alabama  
C. H. Walters, Boiler & Elevator Programs, Portland, Oregon  
M. W. A. West, Department of Fisheries & Labour, Charlottetown, Prince Edward Island, Canada  
T. F. Wickham, Department of Labor, Providence, Rhode Island  
R. A. Yeo, Department of Labour and Manpower, Halifax, Nova Scotia, Canada

### **B31 NATIONAL INTEREST REVIEW GROUP**

Aluminum Association – W. W. Pritsky  
American Boiler Manufacturers Association – R. J. Fletcher  
American Institute of Chemical Engineers – W. C. Carnell  
American Iron and Steel Institute – J. R. Pegues  
American Petroleum Institute, Division of Refining – H. M. Howarth  
American Pipe Fitting Association – J. Thielsch  
American Society of Heating, Refrigeration & Air Conditioning Engineers – H. R. Kornblum  
American Welding Society – H. A. Sosnin  
Chemical Manufacturers Association – D. R. Frikken  
Compressed Gas Association – M. F. Melchioris  
Copper Development Association – A. Cohn  
Ductile Iron Pipe Research Association – T. F. Stroud  
Edison Electric Institute – R. L. Williams  
International District Heating Association – G. Von Bargaen  
Manufacturers Standardization Society of the Valve and Fittings Industry – R. A. Schmidt  
Mechanical Contractors Association of America – W. E. Maloney  
National Association of Plumbing-Heating-Cooling Contractors – R. E. White  
National Association of Regulatory Utility Commissioners – D. W. Snyder  
National Fire Protection Association – T. C. Lemoff  
National Fluid Power Association – H. Anderson  
Naval Sea Systems Command – T. W. Hull  
Pipe Fabrication Institute – L. Katz  
Slurry Transport Association – P. E. Snoek  
Society of Ohio Safety Engineers – J. M. Holleran  
Valve Manufacturers Association – R. A. Handschumacher



## CONTENTS

Foreword .....		iii
Personnel .....		iv
<b>Part 1</b>	<b>Introduction .....</b>	<b>1</b>
1.1	Scope .....	1
1.2	Limitations .....	1
1.3	Initial Development .....	2
1.4	Methodology and Research Procedures .....	2
1.5	How to Use the Manual .....	3
1.6	The Meaning of Acceptance .....	5
1.7	Other Means of Determining Safe Pipeline Operating Pressure .....	5
1.8	Computer Programs .....	5
<b>Figures</b>		
Fig. 1-1	Parabolic Criteria for Classifying Corrosion Defects According to Predicted Failure Stress .....	4
Fig. 1-2	Procedure for Analysis of Corroded Pipe Strength .....	6
<b>Part 2</b>	<b>Determination of Maximum Allowable     Longitudinal Extent of Corrosion .....</b>	<b>9</b>
<b>Figures</b>		
Fig. 2-1	Corrosion Parameters Used in Analysis .....	10
Fig. 2-2	Curve for Determining the Value of <i>B</i> .....	11
<b>Part 3</b>	<b>Tables for Corrosion Limits .....</b>	<b>13</b>
<b>Tables</b>		
Table 3-1	Values of <i>L</i> for Pipe Sizes $\geq$ NPS 2 and $<$ NPS 6 .....	14
Table 3-2	Values of <i>L</i> for Pipe Sizes $\geq$ NPS 6 and $<$ NPS 10 .....	15



Table 3-3	Values of $L$ for Pipe Sizes $\geq$ NPS 10 and $<$ NPS 16 .....	16
Table 3-4	Values of $L$ for Pipe Sizes $\geq$ NPS 16 and $<$ NPS 20 .....	17
Table 3-5	Values of $L$ for Pipe Sizes $\geq$ NPS 20 and $<$ NPS 24 .....	18
Table 3-6	Values of $L$ for Pipe Sizes $\geq$ NPS 24 and $<$ NPS 30 .....	19
Table 3-7	Values of $L$ for Pipe Sizes $\geq$ NPS 30 and $<$ NPS 36 .....	20
Table 3-8	Values of $L$ for Pipe Sizes $\geq$ NPS 36 and $<$ NPS 42 .....	21
Table 3-9	Values of $L$ for Pipe Sizes $\geq$ NPS 42 and $<$ NPS 48 .....	22
Table 3-10	Values of $L$ for Pipe Sizes $\geq$ NPS 48 and $<$ NPS 52 .....	26
Table 3-11	Values of $L$ for Pipe Sizes $\geq$ NPS 52 and $<$ NPS 56 .....	30
Table 3-12	Values of $L$ for Pipe Sizes $\geq$ NPS 56 and $<$ NPS 60 .....	34
<b>Part 4</b>	<b>Evaluation of MAOP in Corroded Area .....</b>	<b>39</b>
4.1	Computation of $A$ .....	39
4.2	Computation of $P'$ .....	39
4.3	MAOP and $P'$ .....	42
<b>Figures</b>		
Fig. 4-1	Curve for Obtaining $P'$ as a Function of $d/t$ for Values of $A$ Less Than or Equal to 4.0 .....	40
Fig. 4-2	$P'$ as a Function of $d/t$ for Values of $A$ Greater Than 4.0 .....	41
<b>Appendices</b>		
Appendix A	BASIC Computer Program, CRVL.BAS, for Determining Allowable Length $L$ (Part 2) or Alternative Maximum Allowable Operating Pressure (Part 4) .....	43
Appendix B	BASIC Computer Program, CRLGTHU.BAS, Used in Generating Tables Like Those Which Are Printed in Part 3 .....	51



This page intentionally left blank.

## PART 1 INTRODUCTION

### 1.1 SCOPE

The scope of this Manual includes all pipelines within the scope of the pipeline codes that are part of ASME B31 Code for Pressure Piping, i.e., ASME B31.4, Liquid Transportation Systems for Hydrocarbons, Liquid Petroleum Gas, Anhydrous Ammonia, and Alcohols; ASME B31.8, Gas Transmission and Distribution Piping Systems; and ASME B31.11, Slurry Transportation Piping Systems. Parts 2, 3, and 4 are based on material included in ASME Guide for Gas Transmission and Distribution Piping Systems, 1983 Edition.

This Manual is not applicable to new construction covered under the B31 Code Sections. That is, it is not intended that this Manual be used to establish acceptance standards for pipe that may have become corroded prior to or during fabrication and/or installation.

This Manual is intended solely for the purpose of providing guideline information for the designer/owner/operator. Thus, the specific use of this Manual is the responsibility of the designer/owner/operator.

### 1.2 LIMITATIONS

(a) This Manual is limited to corrosion on weldable pipeline steels categorized as carbon steels or high strength low alloy steels. Typical of these materials are those described in ASTM A 53, A 106, and A 381, and API 5L. (The current API 5L includes all Grades formerly in API 5LX and 5LS.)

(b) This Manual applies only to defects in the body of line pipe which have relatively smooth contours and cause low stress concentration (e.g., electrolytic or galvanic corrosion, loss of wall thickness due to erosion).

(c) This procedure should not be used to evaluate the remaining strength of corroded girth or longitudinal welds or related heat affected zones, defects caused by mechanical damage, such as gouges and grooves, and defects introduced during pipe or plate manufacture, such as seams, laps, rolled ends, scabs, or slivers.

(d) The criteria for corroded pipe to remain in service presented in this Manual are based only upon the ability of the pipe to maintain structural integrity under internal pressure. It should not be the sole criterion when the pipe is subject to significant secondary stresses (e.g., bending), particularly if the corrosion has a significant transverse component.

(e) This procedure does not predict leaks or rupture failures.



### 1.3 INITIAL DEVELOPMENT

In the late 1960s, a major long-lines gas transmission pipeline company in conjunction with the Battelle Memorial Institute in Columbus, Ohio, began a research effort to examine the fracture initiation behavior of various kinds of corrosion defects in line pipe. This included determining the relationship between the size of a defect and the level of internal pressure that would cause the defect to leak or rupture. The testing by the gas pipeline company and Battelle demonstrated that there was indeed a possibility of developing methodology and procedures to analyze varying degrees of corrosion of existing pipelines. From this, an operator could make a valid determination as to whether the pipelines could safely remain in service or should be repaired or replaced. As the awareness of this research program grew, other transmission companies began to express considerable interest.

Beginning in the early 1970s, the American Gas Association (AGA) Pipeline Research Committee assumed responsibility for this activity and began developing methods for predicting the pressure strength of line pipe containing various sizes of corrosion defects.

The overall objective of these experiments was to examine the fracture initiation behavior of various sizes of corrosion defects by determining the relationship between the size of a defect and the level of internal pressure that would cause a leak or rupture.

### 1.4 METHODOLOGY AND RESEARCH PROCEDURES

The procedure contained in this Manual is based upon pressuring actual corroded pipe to failure in an extensive series of full-size tests. Since there was pipe available that had been removed from service and that had sustained corrosion damage, it seemed more logical to test these full-size, actual field specimens, either in place or in a large, full-scale test cell, rather than base these guidelines upon purely laboratory tests using machined defects. Several hundred full-scale pipe tests were conducted on all types of defects to establish general defect behavior. Mathematical expressions to calculate the pressure strength of corroded pipe materials were developed on the basis of these extensive tests. These mathematical expressions, although semiempirical, were founded upon well established principles of fracture mechanics. The basis principle of fracture mechanics is that the resistance of the material to unstable fracturing in the presence of a defect is related to the size of the defect and an inherent metal property called toughness. The tougher the material, the larger the flaw that can be tolerated before failure will occur. Also, the bigger the defect, the lower the pressure at which a leak or rupture will occur. These two features may seem obvious, but they form the basis of fracture mechanics in terms of determining the real strength of pipe containing defects.

During 1970 and 1971, 47 pressure tests were conducted on several pipe sizes to evaluate the effectiveness of the mathematical expressions in determining the strength of corroded areas. The diameter of the pipe material examined ranged from 16 in. through 30 in. and wall thickness varied from 0.312 in. through 0.375 in. The pipe materials have ranged in yield strength from about 25,000 psi for API 5L Grade A-25 to about 52,000 psi for 5LX Grade X-52.

The mathematical expressions developed from the earlier experiments have been modified based on later test results and now provide reliable estimates of the failure pressures for corrosion defects over the range of materials covered in this study. The experiments



on corroded pipe indicated that line pipe steels have adequate toughness and that the toughness is not a significant factor. The failure of blunt corrosion flaws is controlled by their size and the flow stress or yield stress of the material.

Figure 1-1 shows the relationship between the full-size test failures and the criterion for acceptance of corrosion pits in line pipe. The criterion is that they shall withstand a pressure equal to a stress level of 100% of the specified minimum yield stress (SMYS). The Figure is based on an assured parabolic profile of the corroded regions and presents the maximum corrosion depth, divided by the pipe wall thickness, plotted against the corrosion length, divided by the square root of the pipe radius times wall thickness. Each of the data points plotted represents one full-size pipe experiment on corroded pipe, and the number next to the data point represents the stress at failure pressure expressed as percent SMYS. There are only 3 data points (experiments) that failed at pressure levels below 100% SMYS, indicating the lack of severity of corrosion defects in general (note that all three would be rejected by this criterion). The solid line shown on the Figure is the line that identifies failure pressures of less than 100% SMYS. There are a number of data points that are below this line, but all of them represent failures above 100% SMYS. The fact that these are above 100% SMYS simply indicates that the criterion is very conservative.

The acceptable region in the plot is the shaded region below and to the left of the solid line. The Tables in Part 3 are based on corrosion depths and lengths determined by this solid line. Corrosion pits that have depths and lengths that fall above the curve are not acceptable, in accordance with the criteria presented herein, and the operating pressure either has to be reduced, or the corrosion pit removed or repaired.

## 1.5 HOW TO USE THE MANUAL

Part 2, Determination of Maximum Allowable Longitudinal Extent of Corrosion, sets forth the equations for determining the severity of the corroded areas. It tells the operator how to measure the longitudinal extent and maximum depth of the corroded areas. One can then use Eq. (2) of Part 2 to determine if the corroded area is serious.

However, it is recognized that most field operators will prefer a simpler method of evaluating a corroded area. Therefore, Part 3, Tables for Corrosion Limits, evaluates Eq. (2) and places the results in tabular form. This allows the field operator to make decisions simply by going to a table after measuring the longitudinal extent and maximum depth of the corroded area and making a choice.

Locate the table appropriate for the pipe O.D. and wall thickness. Look down the left column and find the depth of corrosion that is equal to or the next number larger than the measured maximum depth of the corroded area. Read across to the column headed by the wall thickness or next number lower than the pipe's nominal wall thickness to determine the maximum allowable longitudinal extent of the corroded area for the depth of corrosion. If the measured longitudinal extent of the corroded area is equal to or less than the maximum allowable longitudinal extent of the corroded area determined from the Table, the pipe strength is suitable for the present MAOP<sup>1</sup> and is capable of containing a test pressure that will produce a stress of 100% SMYS of the pipe material.

<sup>1</sup>As used in this manual, the term MAOP shall represent maximum steady state operating pressure for pipelines within the scope of ASME B31.4 and ASME B31.11 and maximum allowable operating pressure for pipelines within the scope of ASME B31.8.





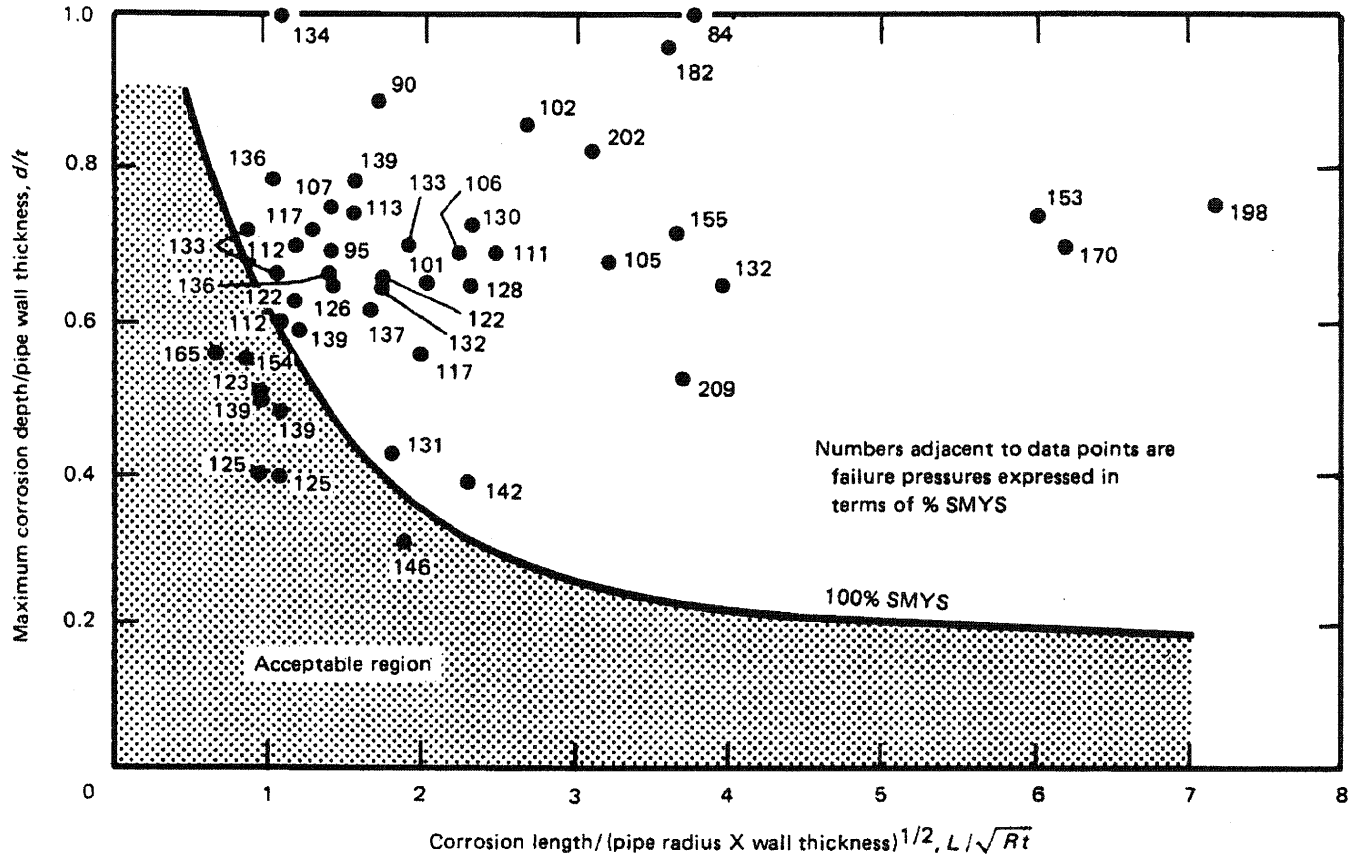


FIG. 1-1 PARABOLIC CRITERIA FOR CLASSIFYING CORROSION DEFECTS ACCORDING TO PREDICTED FAILURE STRESS

The tables produce results which may be more conservative than Eq. (2) of Part 2. The tables could show that the corroded area is unsuitable for the current MAOP, but Eq. (2) may show that it is. Therefore, it is possible for the corroded region to be rejected by the tables, but found suitable by using Eq. (2).

If the tables and Eq. (2) both show the corroded region to be unsuitable, it may still be possible to establish suitability by one of the methods mentioned in para. 1.7. Another alternative would be to lower the MAOP of the pipeline, if permitted by operating conditions. Part 4 can be used to determine a lower MAOP that has the same safety factor provided by Parts 2 and 3.

Regardless of which alternative is chosen, in all cases where the corroded region is to be left in service, measures should be taken to arrest further corrosion. Such measures should include coating the corroded region and, if indicated, increasing the cathodic protection level.

Figure 1-2, Procedure for Analysis of Corroded Pipe Strength, shows the steps necessary to proceed through the evaluation of a corroded area on a pipeline in order to determine if any corrective action is needed. The steps shown in the dashed boxes are valid means of determining a safe operating pressure (or MAOP), but the procedures for conducting these steps or the acceptance levels are not in this Manual.

## 1.6 THE MEANING OF ACCEPTANCE

(a) Any corroded region indicated as acceptable by the criteria of this Manual for service at the established MAOP is capable of withstanding a hydrostatic pressure test that will produce a stress of 100% of the pipe SMYS.

(b) Any corroded region indicated as acceptable for service at a reduced MAOP is capable of withstanding a hydrostatic pressure test at a ratio above the MAOP equal to the ratio of a 100% SMYS test to 72% SMYS operation (1.39:1). If a larger ratio is desired, the reduced MAOP can be adjusted accordingly.

## 1.7 OTHER MEANS OF DETERMINING SAFE PIPELINE OPERATING PRESSURE

(a) The operator can make a more rigorous analysis of the corroded area to determine the remaining strength by performing a fracture mechanics analysis based upon established principles and practices using the actual profile of the corroded region.

(b) The operator can reestablish the MAOP by a complete hydrostatic pressure test that produces a minimum stress of 100% SMYS, or establish a lower MAOP based on the pressure of a successful test conducted at a lower pressure.

(c) The procedures and acceptance criteria for conducting these alternative acceptance tests, either fracture mechanics analysis or hydrostatic tests, are not included in this Manual.

## 1.8 COMPUTER PROGRAMS

Appendix A is a BASIC computer program, CRVL.BAS, developed by Mr. Richard L. Seifert and is based on the equations in Parts 2 and 4. It can be used to expedite the evaluation procedure. Several examples of the program output are shown.



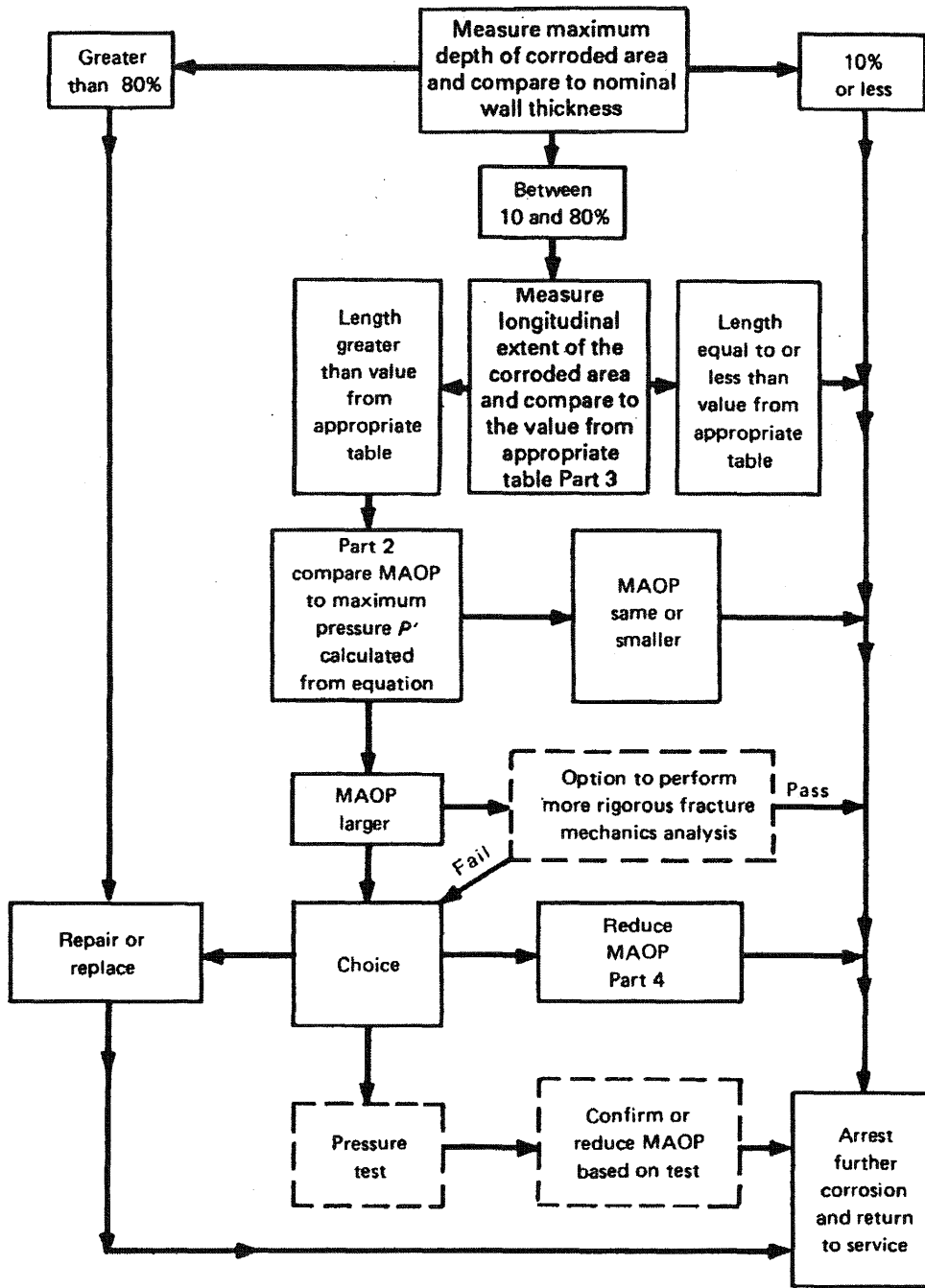


FIG. 1-2 PROCEDURE FOR ANALYSIS OF CORRODED PIPE STRENGTH

Appendix B is a BASIC computer program, CRLGTHU.BAS by Mr. Seifert, which is an upgrade of CRLGTH.BAS, which was contained in the first printing of this Manual. CRLGTH.BAS was used to produce some of the tables in Part 3. It required that the BASIC program be modified slightly each time it was used. The new program CRLGTHU.BAS does not require modification. It will produce a printed table of maximum acceptable corrosion lengths for a given pipe diameter, and up to ten wall thicknesses of that diameter. An example of a printed table by this program is included at the end of Appendix B.

Both CRVL.BAS and CRLGTHU.BAS were written in BASIC for a specific computer/printer combination and can be utilized by most state-of-the-art microprocessors. However, minor modifications may be necessary for use on other equipment or for other purposes.

These computer programs are reproduced herein solely for the convenience of the Manual user, and ASME and the author make no claims as to their accuracy or effectiveness.



This page intentionally left blank.



**PART 2**  
**DETERMINATION OF MAXIMUM ALLOWABLE**  
**LONGITUDINAL EXTENT OF CORROSION**

The depth of a corrosion pit may be expressed as a percent of the nominal wall thickness of the pipe by:

$$\% \text{ pit depth} = 100d/t \quad (1)$$

where

$d$  = measured maximum depth of the corroded area, in., as shown in Fig. 2-1

$t$  = nominal wall thickness of the pipe, in. Additional wall thickness required for concurrent external loads shall not be included in the calculations.

A contiguous corroded area having a maximum depth of more than 10% but less than 80% of the nominal wall thickness of the pipe should not extend along the longitudinal axis of the pipe for a distance greater than that calculated from:

$$L = 1.12B\sqrt{Dt} \quad (2)$$

( $L$  may also be determined from Tables 3-1 through 3-12 in Part 3.)

where

$L$  = maximum allowable longitudinal extent of the corroded area, in., collinear with  $L_M$  in Fig. 2-1

$D$  = nominal outside diameter of the pipe, in.

$B$  = a value which may be determined from the curve in Fig. 2-2 or from:

$$B = \sqrt{\left(\frac{d/t}{1.1 d/t - 0.15}\right)^2 - 1} \quad (3)$$

except that  $B$  may not exceed the value 4. If the corrosion depth is between 10% and 17.5%, use  $B = 4.0$  in Eq. (2).



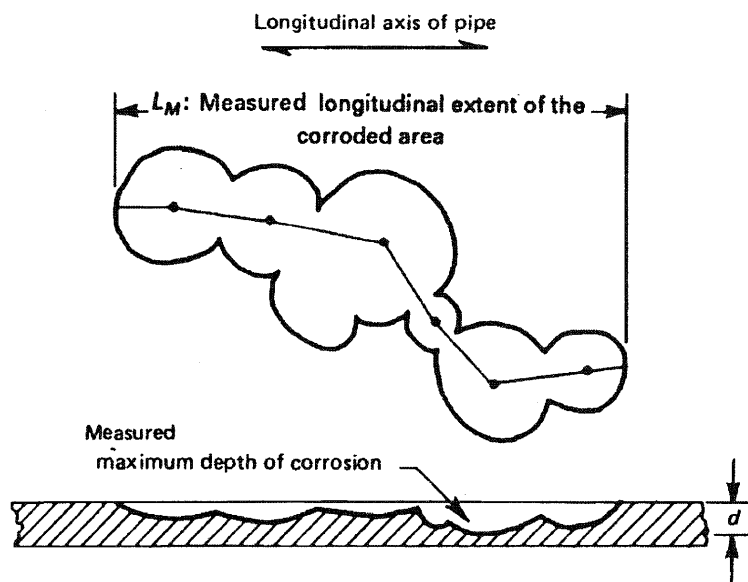


FIG. 2-1 CORROSION PARAMETERS USED IN ANALYSIS

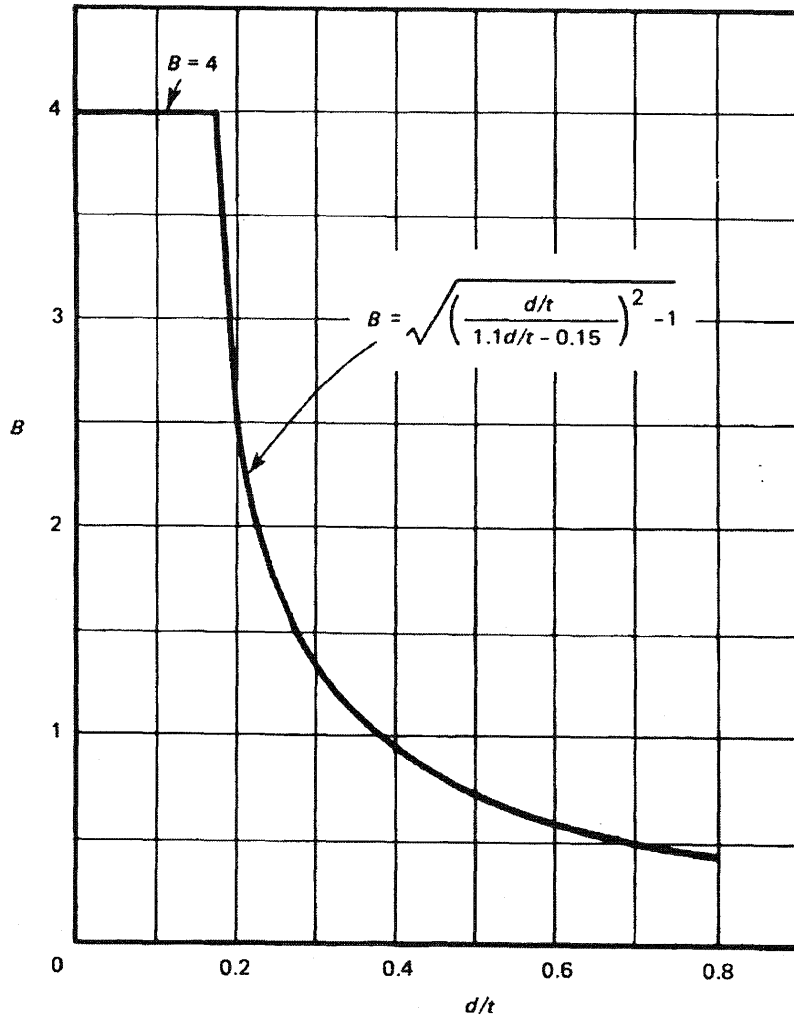


FIG. 2-2 CURVE FOR DETERMINING THE VALUE  $B$



This page intentionally left blank.



### PART 3 TABLES FOR CORROSION LIMITS

The tables in this Part are calculated from the equations in Part 2. They provide a ready reference of maximum corrosion lengths for a spectrum of pipe diameters, wall thicknesses, and pit depths. These Tables may be used to determine the maximum allowable longitudinal extent of a contiguous area of corrosion as given in Part 2.

(a) The corroded area must be clean to bare metal. Care should be taken when cleaning corroded areas of a pressurized pipeline.

(b) Measure the maximum depth of the corroded area  $d$  and the longitudinal extent of the corroded area as shown in Fig. 2-1.

(c) Determine the size (NPS) of the pipe and nominal wall thickness.

(d) Turn to the page in the Table corresponding to the size (NPS) of the pipe.

(e) Locate the row showing a depth equal to the measured maximum depth of the corroded area. If the exact measured value is not listed, choose the row showing the NEXT GREATER DEPTH.

(f) Scan across to the column showing the wall thickness of the pipe. If the nominal wall thickness is not listed, use the column for the NEXT THINNER WALL. The value  $L$  found at the intersection of the wall thickness column and depth row is the maximum allowable longitudinal extent of such a corroded area.

(g) The tables in Part 3 produce results which may be more conservative than those obtained from the equations in Part 2. Therefore, the tables could show that a given corroded area is unsuitable for the current MAOP, but the use of the equations in Part 2 may show that it is acceptable.



TABLE 3-1 VALUES OF  $L$  FOR PIPE SIZES  $\geq$  NPS 2 AND  $<$  NPS 6

Depth, $d$ , in.	Wall Thickness, $t$ , in.							
	0.083	0.109	0.125	0.141	0.154	0.172	0.188	0.218
0.01	2	.....	.....	.....	.....	.....	.....	.....
0.02	$1\frac{5}{16}$	$1\frac{15}{16}$	$2\frac{7}{16}$	$2\frac{3}{16}$	$2\frac{11}{16}$	$2\frac{7}{8}$	3	.....
0.03	$\frac{1}{2}$	$\frac{7}{8}$	$1\frac{1}{8}$	$1\frac{1}{2}$	$1\frac{15}{16}$	$2\frac{7}{8}$	3	$3\frac{1}{4}$
0.04	$\frac{3}{8}$	$\frac{5}{8}$	$\frac{3}{4}$	$1\frac{5}{16}$	$1\frac{1}{8}$	$1\frac{3}{8}$	$1\frac{3}{4}$	$2\frac{3}{4}$
0.05	$\frac{5}{16}$	$\frac{7}{16}$	$\frac{9}{16}$	$1\frac{1}{16}$	$1\frac{3}{16}$	1	$1\frac{3}{16}$	$1\frac{5}{8}$
0.06	$\frac{1}{4}$	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{5}{16}$	$1\frac{1}{16}$	$1\frac{3}{16}$	$1\frac{5}{16}$	$1\frac{3}{16}$
0.07	.....	$\frac{5}{16}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$1\frac{1}{16}$	$\frac{3}{4}$	1
0.08	.....	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$1\frac{1}{16}$	$1\frac{3}{16}$
0.09	.....	.....	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{3}{4}$
0.10	.....	.....	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$1\frac{1}{16}$
0.11	.....	.....	.....	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{5}{8}$
0.12	.....	.....	.....	.....	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{9}{16}$
0.13	.....	.....	.....	.....	.....	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{1}{2}$
0.14	.....	.....	.....	.....	.....	.....	$\frac{3}{8}$	$\frac{7}{16}$
0.15	.....	.....	.....	.....	.....	.....	$\frac{5}{16}$	$\frac{7}{16}$
0.16	.....	.....	.....	.....	.....	.....	.....	$\frac{3}{8}$
0.17	.....	.....	.....	.....	.....	.....	.....	$\frac{3}{8}$



**TABLE 3-2 VALUES OF L FOR PIPE SIZES ≥ NPS 6 AND < NPS 10**

Depth, d, in.	Wall Thickness, t, in.							
	0.083	0.125	0.156	0.188	0.203	0.219	0.250	0.312
0.010	3 <sup>5</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	.....	.....
0.020	1 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>4</sup> / <sub>16</sub>	5	.....	.....	.....	.....
0.030	7 <sup>8</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>	5	5 <sup>3</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>4</sub>	.....
0.040	5 <sup>8</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sup>7</sup> / <sub>8</sub>	2 <sup>15</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>7</sup> / <sub>16</sub>
0.050	1 <sup>1</sup> / <sub>2</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>8</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>7</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>16</sub>
0.060	7 <sup>8</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>8</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>11</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>
0.070	.....	1 <sup>1</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>11</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>
0.080	.....	9 <sup>16</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>4</sub>	2 <sup>11</sup> / <sub>16</sub>
0.090	.....	1 <sup>1</sup> / <sub>2</sub>	3 <sup>4</sup> / <sub>8</sub>	1	1 <sup>1</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>
0.100	.....	7 <sup>16</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	7 <sup>8</sup> / <sub>16</sub>	1	1 <sup>1</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>8</sub>	2
0.110	.....	.....	9 <sup>16</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	7 <sup>8</sup> / <sub>16</sub>	1	1 <sup>1</sup> / <sub>4</sub>	1 <sup>3</sup> / <sub>4</sub>
0.120	.....	.....	9 <sup>16</sup> / <sub>16</sub>	3 <sup>4</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>
0.130	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	3 <sup>4</sup> / <sub>8</sub>	7 <sup>8</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>
0.140	.....	.....	.....	5 <sup>8</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>8</sub>
0.150	.....	.....	.....	9 <sup>16</sup> / <sub>16</sub>	5 <sup>8</sup> / <sub>16</sub>	3 <sup>4</sup> / <sub>8</sub>	7 <sup>8</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>4</sub>
0.160	.....	.....	.....	.....	9 <sup>16</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>
0.170	.....	.....	.....	.....	.....	5 <sup>8</sup> / <sub>16</sub>	3 <sup>4</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>8</sub>
0.180	.....	.....	.....	.....	.....	.....	3 <sup>4</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>
0.190	.....	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	1
0.200	.....	.....	.....	.....	.....	.....	5 <sup>8</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>16</sub>
0.210	.....	.....	.....	.....	.....	.....	.....	7 <sup>8</sup> / <sub>16</sub>
0.220	.....	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>16</sub>
0.230	.....	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>16</sub>
0.240	.....	.....	.....	.....	.....	.....	.....	3 <sup>4</sup> / <sub>8</sub>

TABLE 3-3 VALUES OF L FOR PIPE SIZES  $\geq$  NPS 10 AND  $<$  NPS 16

Depth, d, in.	Wall Thickness, t, in.							
	0.156	0.219	0.250	0.307	0.344	0.365	0.438	0.500
0.020	5 <sup>13</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	.....	.....
0.030	4 <sup>5</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>8</sub>	.....	.....	.....	.....	.....
0.040	2 <sup>7</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>8</sub>	8 <sup>8</sup> / <sub>8</sub>	8 <sup>8</sup> / <sub>8</sub>	.....	.....
0.050	1 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>8</sub>	8 <sup>8</sup> / <sub>8</sub>	8 <sup>7</sup> / <sub>8</sub>	9 <sup>3</sup> / <sub>4</sub>	10 <sup>3</sup> / <sub>8</sub>
0.060	1 <sup>7</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>4</sub>	8 <sup>8</sup> / <sub>8</sub>	8 <sup>8</sup> / <sub>8</sub>	9 <sup>3</sup> / <sub>4</sub>	10 <sup>3</sup> / <sub>8</sub>
0.070	1 <sup>3</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>2</sub>	6 <sup>5</sup> / <sub>8</sub>	9 <sup>3</sup> / <sub>4</sub>	10 <sup>3</sup> / <sub>8</sub>
0.080	1 <sup>1</sup> / <sub>16</sub>	1 <sup>13</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	8 <sup>3</sup> / <sub>8</sub>	10 <sup>3</sup> / <sub>8</sub>
0.090	1 <sup>5</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>16</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>13</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	9 <sup>3</sup> / <sub>8</sub>
0.100	1 <sup>3</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>4</sub>	2 <sup>7</sup> / <sub>16</sub>	3	3 <sup>3</sup> / <sub>8</sub>	4 <sup>15</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>
0.110	3 <sup>1</sup> / <sub>4</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>5</sup> / <sub>8</sub>	2 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>
0.120	1 <sup>1</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	2	2 <sup>3</sup> / <sub>8</sub>	2 <sup>5</sup> / <sub>8</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>
0.130	.....	1	1 <sup>5</sup> / <sub>16</sub>	1 <sup>13</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>8</sub>	3 <sup>5</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>
0.140	.....	1 <sup>5</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sup>11</sup> / <sub>16</sub>	2	2 <sup>3</sup> / <sub>16</sub>	3	3 <sup>3</sup> / <sub>16</sub>
0.150	.....	7 <sup>7</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>8</sub>	1 <sup>9</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>7</sup> / <sub>16</sub>
0.160	.....	1 <sup>3</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>4</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>
0.170	.....	3 <sup>1</sup> / <sub>4</sub>	1	1 <sup>3</sup> / <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	1 <sup>13</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>8</sub>	2 <sup>15</sup> / <sub>16</sub>
0.180	.....	.....	1 <sup>5</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>16</sub>	1 <sup>11</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>	2 <sup>3</sup> / <sub>4</sub>
0.190	.....	.....	7 <sup>7</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>5</sup> / <sub>8</sub>
0.200	.....	.....	1 <sup>13</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>2</sub>	2	2 <sup>7</sup> / <sub>16</sub>
0.210	.....	.....	.....	1 <sup>1</sup> / <sub>8</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>8</sub>	2 <sup>3</sup> / <sub>16</sub>
0.220	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sup>3</sup> / <sub>8</sub>	1 <sup>13</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>
0.230	.....	.....	.....	1	1 <sup>3</sup> / <sub>16</sub>	1 <sup>5</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>8</sub>
0.240	.....	.....	.....	1 <sup>5</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sup>11</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>
0.250	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	1 <sup>15</sup> / <sub>16</sub>
0.260	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>2</sub>	1 <sup>7</sup> / <sub>8</sub>
0.270	.....	.....	.....	.....	1	1 <sup>1</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>13</sup> / <sub>16</sub>
0.280	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>4</sub>
0.290	.....	.....	.....	.....	.....	1	1 <sup>3</sup> / <sub>8</sub>	1 <sup>11</sup> / <sub>16</sub>
0.300	.....	.....	.....	.....	.....	.....	1 <sup>5</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>8</sub>
0.310	.....	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>4</sub>	1 <sup>9</sup> / <sub>16</sub>
0.320	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>2</sub>
0.330	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>
0.340	.....	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>8</sub>
0.350	.....	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>8</sub>
0.360	.....	.....	.....	.....	.....	.....	.....	1 <sup>9</sup> / <sub>16</sub>
0.370	.....	.....	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>4</sub>
0.380	.....	.....	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>4</sub>
0.390	.....	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>16</sub>
0.400	.....	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>16</sub>
0.410	.....	.....	.....	.....	.....	.....	.....	.....



**TABLE 3-4 VALUES OF L FOR PIPE SIZES ≥ NPS 16 AND < NPS 20**

Depth, d, in.	Wall Thickness, t, in.							
	0.188	0.250	0.312	0.344	0.375	0.438	0.500	0.625
0.020	7/8	.....	.....	.....	.....	.....	.....	.....
0.030	7/8	8 1/16	.....	.....	.....	.....	.....	.....
0.040	4 1/2	8 1/16	10	10 1/2	11	.....	.....	.....
0.050	3 1/16	6	10	10 1/2	11	11 1/8	12 1/16	.....
0.060	2 3/8	4 1/8	7 1/8	10 1/2	11	11 1/8	12 1/16	.....
0.070	2	3 1/4	5 1/4	6 3/4	8 13/16	11 1/8	12 1/16	14 3/8
0.080	1 3/4	2 3/4	4 3/8	5 1/8	6 3/8	10 1/16	12 1/16	14 3/8
0.090	1 1/2	2 3/8	3 1/2	4 1/4	5 1/8	7 1/16	11 1/16	14 3/8
0.100	1 3/8	2 1/8	3 1/16	3 5/8	4 5/16	6	8 1/2	14 3/8
0.110	1 1/4	1 15/16	2 3/4	3 1/4	3 3/4	5 1/8	6 3/8	13 7/8
0.120	1 1/8	1 3/4	2 1/2	2 15/16	3 3/8	4 1/2	5 7/8	10 9/16
0.130	1 1/16	1 5/8	2 1/4	2 11/16	3 1/16	4	5 3/16	8 5/8
0.140	1 5/16	1 1/2	2 1/8	2 7/16	2 13/16	3 5/8	4 5/8	7 1/16
0.150	7/8	1 3/8	1 15/16	2 1/4	2 5/8	3 3/8	4 1/4	6 9/16
0.160	.....	1 5/16	1 13/16	2 1/8	2 7/16	3 3/8	3 7/8	5 15/16
0.170	.....	1 3/16	1 11/16	2	2 1/4	2 5/16	3 5/8	5 3/8
0.180	.....	1 1/8	1 5/8	1 7/8	2 1/8	2 3/4	3 3/8	5
0.190	.....	1 1/16	1 1/2	1 3/4	2	2 1/16	3 3/16	4 5/8
0.200	.....	1	1 7/16	1 11/16	1 15/16	2 7/16	3	4 3/8
0.210	.....	.....	1 3/8	1 5/8	1 13/16	2 5/16	2 7/8	4 1/8
0.220	.....	.....	1 3/16	1 1/2	1 3/4	2 3/16	2 11/16	3 7/8
0.230	.....	.....	1 1/4	1 7/16	1 11/16	2 1/8	2 9/16	3 1/16
0.240	.....	.....	1 3/16	1 3/8	1 9/16	2	2 1/2	3 1/2
0.250	.....	.....	.....	1 5/16	1 1/2	1 15/16	2 3/8	3 3/8
0.260	.....	.....	.....	1 1/4	1 7/16	1 7/8	2 1/4	3 1/4
0.270	.....	.....	.....	1 3/16	1 3/8	1 13/16	2 3/16	3 1/8
0.280	.....	.....	.....	.....	1 5/16	1 11/16	2 1/8	3
0.290	.....	.....	.....	.....	1 3/16	1 5/8	2 1/16	2 7/8
0.300	.....	.....	.....	.....	1 1/4	1 9/16	1 15/16	2 3/4
0.310	.....	.....	.....	.....	.....	1 9/16	1 7/8	2 1/16
0.320	.....	.....	.....	.....	.....	1 1/2	1 13/16	2 1/16
0.330	.....	.....	.....	.....	.....	1 7/16	1 3/4	2 1/2
0.340	.....	.....	.....	.....	.....	1 3/8	1 11/16	2 7/16
0.350	.....	.....	.....	.....	.....	1 5/16	1 11/16	2 3/8
0.360	.....	.....	.....	.....	.....	.....	1 5/8	2 5/16
0.370	.....	.....	.....	.....	.....	.....	1 9/16	2 1/4
0.380	.....	.....	.....	.....	.....	.....	1 1/2	2 3/16
0.390	.....	.....	.....	.....	.....	.....	1 7/16	2 1/8
0.400	.....	.....	.....	.....	.....	.....	1 5/16	2 1/16
0.410	.....	.....	.....	.....	.....	.....	.....	2
0.420	.....	.....	.....	.....	.....	.....	.....	1 15/16
0.430	.....	.....	.....	.....	.....	.....	.....	1 7/8
0.440	.....	.....	.....	.....	.....	.....	.....	1 7/8
0.450	.....	.....	.....	.....	.....	.....	.....	1 13/16
0.460	.....	.....	.....	.....	.....	.....	.....	1 3/4
0.470	.....	.....	.....	.....	.....	.....	.....	1 11/16
0.480	.....	.....	.....	.....	.....	.....	.....	1 11/16
0.490	.....	.....	.....	.....	.....	.....	.....	1 5/8
0.500	.....	.....	.....	.....	.....	.....	.....	1 9/16
0.510	.....	.....	.....	.....	.....	.....	.....	.....

**TABLE 3-5 VALUES OF L FOR PIPE SIZES ≥ NPS 20 AND < NPS 24**

Depth, d, in.	Wall Thickness, t, in.							
	0.219	0.250	0.344	0.406	0.469	0.500	0.562	0.625
0.030	9 <sup>3</sup> / <sub>16</sub>	10	.....	.....	.....	.....	.....	.....
0.040	8 <sup>1</sup> / <sub>16</sub>	10	11 <sup>3</sup> / <sub>4</sub>	.....	.....	.....	.....	.....
0.050	4 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>16</sub>	11 <sup>3</sup> / <sub>4</sub>	12 <sup>3</sup> / <sub>4</sub>	13 <sup>3</sup> / <sub>4</sub>	14 <sup>3</sup> / <sub>16</sub>	.....	.....
0.060	3 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	11 <sup>3</sup> / <sub>4</sub>	12 <sup>3</sup> / <sub>4</sub>	13 <sup>3</sup> / <sub>4</sub>	14 <sup>3</sup> / <sub>16</sub>	15	.....
0.070	2 <sup>7</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>4</sub>	13 <sup>3</sup> / <sub>4</sub>	14 <sup>3</sup> / <sub>16</sub>	15	15 <sup>13</sup> / <sub>16</sub>
0.080	2 <sup>7</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	8 <sup>7</sup> / <sub>8</sub>	13 <sup>3</sup> / <sub>4</sub>	14 <sup>3</sup> / <sub>16</sub>	15	15 <sup>13</sup> / <sub>16</sub>
0.090	2 <sup>3</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	6 <sup>13</sup> / <sub>16</sub>	10 <sup>3</sup> / <sub>16</sub>	12 <sup>13</sup> / <sub>16</sub>	15	15 <sup>13</sup> / <sub>16</sub>
0.100	1 <sup>15</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	7 <sup>15</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>2</sub>	14 <sup>1</sup> / <sub>8</sub>	15 <sup>13</sup> / <sub>16</sub>
0.110	1 <sup>3</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>8</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>8</sub>	7 <sup>1</sup> / <sub>16</sub>	10 <sup>5</sup> / <sub>8</sub>	15 <sup>1</sup> / <sub>2</sub>
0.120	1 <sup>3</sup> / <sub>8</sub>	1 <sup>15</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	11 <sup>3</sup> / <sub>4</sub>
0.130	1 <sup>1</sup> / <sub>2</sub>	1 <sup>13</sup> / <sub>16</sub>	3	3 <sup>15</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	7 <sup>7</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>
0.140	1 <sup>3</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>16</sub>
0.150	1 <sup>1</sup> / <sub>4</sub>	1 <sup>9</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>7</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>16</sub>
0.160	1 <sup>3</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>8</sub>
0.170	1 <sup>1</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>4</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>
0.180	.....	1 <sup>1</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>
0.190	.....	1 <sup>3</sup> / <sub>16</sub>	2	2 <sup>9</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>16</sub>
0.200	.....	1 <sup>1</sup> / <sub>8</sub>	1 <sup>7</sup> / <sub>8</sub>	2 <sup>7</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>
0.210	.....	.....	1 <sup>13</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>
0.220	.....	.....	1 <sup>1</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>
0.230	.....	.....	1 <sup>5</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>5</sup> / <sub>8</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>8</sub>
0.240	.....	.....	1 <sup>9</sup> / <sub>16</sub>	2	2 <sup>1</sup> / <sub>2</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>
0.250	.....	.....	1 <sup>1</sup> / <sub>2</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>
0.260	.....	.....	1 <sup>7</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>8</sub>	2 <sup>5</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>8</sub>
0.270	.....	.....	1 <sup>3</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>4</sub>	2 <sup>7</sup> / <sub>16</sub>	2 <sup>15</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>
0.280	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>3</sup> / <sub>8</sub>	2 <sup>13</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>
0.290	.....	.....	.....	1 <sup>5</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>16</sub>
0.300	.....	.....	.....	1 <sup>9</sup> / <sub>16</sub>	2	2 <sup>3</sup> / <sub>16</sub>	2 <sup>5</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>8</sub>
0.310	.....	.....	.....	1 <sup>1</sup> / <sub>2</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>9</sup> / <sub>16</sub>	3
0.320	.....	.....	.....	1 <sup>7</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>
0.330	.....	.....	.....	.....	1 <sup>13</sup> / <sub>16</sub>	2	2 <sup>3</sup> / <sub>8</sub>	2 <sup>13</sup> / <sub>16</sub>
0.340	.....	.....	.....	.....	1 <sup>3</sup> / <sub>4</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>5</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>
0.350	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	1 <sup>7</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>4</sub>	2 <sup>5</sup> / <sub>8</sub>
0.360	.....	.....	.....	.....	1 <sup>5</sup> / <sub>8</sub>	1 <sup>13</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>
0.370	.....	.....	.....	.....	1 <sup>9</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>2</sub>
0.380	.....	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>16</sub>
0.390	.....	.....	.....	.....	.....	1 <sup>5</sup> / <sub>8</sub>	2	2 <sup>3</sup> / <sub>8</sub>
0.400	.....	.....	.....	.....	.....	1 <sup>9</sup> / <sub>16</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>5</sup> / <sub>16</sub>
0.410	.....	.....	.....	.....	.....	.....	1 <sup>7</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>4</sub>
0.420	.....	.....	.....	.....	.....	.....	1 <sup>13</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>
0.430	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>8</sub>
0.440	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>16</sub>
0.450	.....	.....	.....	.....	.....	.....	.....	2
0.460	.....	.....	.....	.....	.....	.....	.....	1 <sup>15</sup> / <sub>16</sub>
0.470	.....	.....	.....	.....	.....	.....	.....	1 <sup>15</sup> / <sub>16</sub>
0.480	.....	.....	.....	.....	.....	.....	.....	1 <sup>7</sup> / <sub>8</sub>
0.490	.....	.....	.....	.....	.....	.....	.....	1 <sup>13</sup> / <sub>16</sub>
0.500	.....	.....	.....	.....	.....	.....	.....	1 <sup>3</sup> / <sub>4</sub>
0.510	.....	.....	.....	.....	.....	.....	.....	.....

**TABLE 3-6 VALUES OF L FOR PIPE SIZES ≥ NPS 24 AND < NPS 30**

Depth, d, in.	Wall Thickness, t, in.							
	0.250	0.312	0.375	0.438	0.469	0.500	0.562	0.625
0.030	11	.....	.....	.....	.....	.....	.....	.....
0.040	11	12¼	13⅞	.....	.....	.....	.....	.....
0.050	7⅝	12¼	13⅞	14½	15	15½	.....	.....
0.060	5⅞	9⅞	13⅞	14½	15	15½	16⅞	.....
0.070	4	6⅞	10⅞	14½	15	15½	16⅞	17⅞
0.080	3⅞	5⅞	7⅞	12½	15	15½	16⅞	17⅞
0.090	2⅞	4⅞	6⅞	9⅞	11⅞	14	16⅞	17⅞
0.100	2⅞	3⅞	5⅞	7⅞	8⅞	10⅞	15⅞	17⅞
0.110	2⅞	3⅞	4⅞	6⅞	7⅞	8⅞	11⅞	16⅞
0.120	2⅞	3⅞	4⅞	5½	6⅞	7⅞	9½	12⅞
0.130	2	2⅞	3⅞	4⅞	5⅞	6⅞	8⅞	10⅞
0.140	1⅞	2⅞	3⅞	4⅞	5⅞	5⅞	7⅞	9⅞
0.150	1⅞	2⅞	3⅞	4⅞	4⅞	5⅞	6⅞	8⅞
0.160	1⅞	2⅞	3	3⅞	4⅞	4⅞	5⅞	7⅞
0.170	1½	2⅞	2⅞	3⅞	4	4⅞	5⅞	6⅞
0.180	1⅞	2	2⅞	3⅞	3⅞	4⅞	5⅞	6⅞
0.190	1⅞	1⅞	2⅞	3⅞	3⅞	3⅞	4⅞	5⅞
0.200	1¼	1⅞	2⅞	3	3⅞	3⅞	4⅞	5⅞
0.210	.....	1⅞	2⅞	2⅞	3⅞	3½	4⅞	5
0.220	.....	1⅞	2⅞	2⅞	3	3⅞	4	4⅞
0.230	.....	1½	2⅞	2⅞	2⅞	3⅞	3⅞	4½
0.240	.....	1⅞	1⅞	2½	2⅞	3⅞	3⅞	4⅞
0.250	.....	.....	1⅞	2⅞	2⅞	2⅞	3½	4⅞
0.260	.....	.....	1⅞	2⅞	2⅞	2⅞	3⅞	3⅞
0.270	.....	.....	1⅞	2⅞	2⅞	2⅞	3⅞	3⅞
0.280	.....	.....	1⅞	2⅞	2⅞	2⅞	3⅞	3⅞
0.290	.....	.....	1⅞	2	2⅞	2½	3	3½
0.300	.....	.....	1½	1⅞	2⅞	2⅞	2⅞	3⅞
0.310	.....	.....	.....	1⅞	2⅞	2⅞	2⅞	3¼
0.320	.....	.....	.....	1⅞	2	2¼	2⅞	3⅞
0.330	.....	.....	.....	1¼	1⅞	2⅞	2⅞	3⅞
0.340	.....	.....	.....	1⅞	1⅞	2⅞	2½	3
0.350	.....	.....	.....	1⅞	1⅞	2⅞	2⅞	2⅞
0.360	.....	.....	.....	.....	1¼	2	2⅞	2⅞
0.370	.....	.....	.....	.....	1⅞	1⅞	2⅞	2¼
0.380	.....	.....	.....	.....	.....	1⅞	2¼	2⅞
0.390	.....	.....	.....	.....	.....	1⅞	2⅞	2⅞
0.400	.....	.....	.....	.....	.....	1¼	2⅞	2½
0.410	.....	.....	.....	.....	.....	.....	2⅞	2⅞
0.420	.....	.....	.....	.....	.....	.....	2	2⅞
0.430	.....	.....	.....	.....	.....	.....	1⅞	2⅞
0.440	.....	.....	.....	.....	.....	.....	1⅞	2¼
0.450	.....	.....	.....	.....	.....	.....	.....	2⅞
0.460	.....	.....	.....	.....	.....	.....	.....	2⅞
0.470	.....	.....	.....	.....	.....	.....	.....	2⅞
0.480	.....	.....	.....	.....	.....	.....	.....	2⅞
0.490	.....	.....	.....	.....	.....	.....	.....	2
0.500	.....	.....	.....	.....	.....	.....	.....	1⅞
0.510	.....	.....	.....	.....	.....	.....	.....	.....



TABLE 3-7 VALUES OF  $L$  FOR PIPE SIZES  $\geq$  NPS 30 AND  $<$  NPS 36

Depth, $d$ , in.	Wall Thickness, $t$ , in.						
	0.250	0.312	0.375	0.438	0.500	0.625	0.688
0.030	12¼	.....	.....	.....	.....	.....	.....
0.040	12¼	13 <sup>11</sup> / <sub>16</sub>	15	.....	.....	.....	.....
0.050	8 <sup>3</sup> / <sub>16</sub>	13 <sup>11</sup> / <sub>16</sub>	15	16¼	17¾	.....	.....
0.060	5 <sup>11</sup> / <sub>16</sub>	10½	15	16¼	17¾	.....	.....
0.070	4½	7¾	12½	16¼	17¾	19¾	20¾
0.080	3¾	5 <sup>11</sup> / <sub>16</sub>	8 <sup>11</sup> / <sub>16</sub>	14	17¾	19¾	20¾
0.090	3¾	4 <sup>13</sup> / <sub>16</sub>	6 <sup>15</sup> / <sub>16</sub>	10¾	15 <sup>11</sup> / <sub>16</sub>	19¾	20¾
0.100	2 <sup>15</sup> / <sub>16</sub>	4¾	5¾	8¾	11¾	19¾	20¾
0.110	2¾	3¾	5¾	7	9 <sup>7</sup> / <sub>16</sub>	18 <sup>15</sup> / <sub>16</sub>	20¾
0.120	2¾	3¾	4¾	6¾	8 <sup>1</sup> / <sub>16</sub>	14 <sup>7</sup> / <sub>16</sub>	20¾
0.130	2¾	3¾	4¾	5½	7 <sup>1</sup> / <sub>16</sub>	11¾	15 <sup>13</sup> / <sub>16</sub>
0.140	2 <sup>1</sup> / <sub>16</sub>	2¾	3¾	5	6¾	10¾	13 <sup>1</sup> / <sub>16</sub>
0.150	1¾	2 <sup>11</sup> / <sub>16</sub>	3¾	4¾	5 <sup>13</sup> / <sub>16</sub>	9	11¼
0.160	1¾	2½	3¾	4¼	5¾	8 <sup>1</sup> / <sub>16</sub>	9 <sup>15</sup> / <sub>16</sub>
0.170	1 <sup>11</sup> / <sub>16</sub>	2¾	3¾	4	4 <sup>15</sup> / <sub>16</sub>	7¾	9
0.180	1¾	2¾	2 <sup>15</sup> / <sub>16</sub>	3¾	4¾	6 <sup>13</sup> / <sub>16</sub>	8¾
0.190	1 <sup>7</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	2¾	3¾	4¾	6¾	7 <sup>7</sup> / <sub>16</sub>
0.200	1¾	2	2¾	3¾	4¾	5 <sup>15</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>
0.210	.....	1¾	2½	3¾	3 <sup>15</sup> / <sub>16</sub>	5¾	6¾
0.220	.....	1 <sup>13</sup> / <sub>16</sub>	2¾	3	3¾	5 <sup>1</sup> / <sub>16</sub>	6¼
0.230	.....	1 <sup>11</sup> / <sub>16</sub>	2¼	2¾	3¾	5 <sup>1</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>
0.240	.....	1¾	2¾	2¾	3¾	4 <sup>13</sup> / <sub>16</sub>	5¾
0.250	.....	.....	2 <sup>1</sup> / <sub>16</sub>	2¾	3¼	4¾	5¾
0.260	.....	.....	2	2 <sup>9</sup> / <sub>16</sub>	3¾	4 <sup>7</sup> / <sub>16</sub>	5¾
0.270	.....	.....	1 <sup>15</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>16</sub>	3	4¼	4 <sup>15</sup> / <sub>16</sub>
0.280	.....	.....	1 <sup>13</sup> / <sub>16</sub>	2¾	2¾	4 <sup>1</sup> / <sub>16</sub>	4¾
0.290	.....	.....	1¾	2¼	2 <sup>13</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>
0.300	.....	.....	1 <sup>11</sup> / <sub>16</sub>	2¾	2 <sup>11</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4¾
0.310	.....	.....	.....	2¾	2¾	3 <sup>11</sup> / <sub>16</sub>	4¼
0.320	.....	.....	.....	2	2½	3 <sup>9</sup> / <sub>16</sub>	4¾
0.330	.....	.....	.....	1 <sup>15</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	4
0.340	.....	.....	.....	1¾	2¾	3 <sup>5</sup> / <sub>16</sub>	3¾
0.350	.....	.....	.....	1 <sup>13</sup> / <sub>16</sub>	2¼	3¼	3¾
0.360	.....	.....	.....	.....	2 <sup>3</sup> / <sub>16</sub>	3¾	3¾
0.370	.....	.....	.....	.....	2½	3 <sup>1</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>
0.380	.....	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>	2 <sup>15</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>
0.390	.....	.....	.....	.....	2	2¾	3¾
0.400	.....	.....	.....	.....	1 <sup>15</sup> / <sub>16</sub>	2 <sup>13</sup> / <sub>16</sub>	3¼
0.410	.....	.....	.....	.....	.....	2¾	3 <sup>1</sup> / <sub>16</sub>
0.420	.....	.....	.....	.....	.....	2 <sup>11</sup> / <sub>16</sub>	3¾
0.430	.....	.....	.....	.....	.....	2 <sup>9</sup> / <sub>16</sub>	3
0.440	.....	.....	.....	.....	.....	2½	2 <sup>15</sup> / <sub>16</sub>
0.450	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>16</sub>	2¾
0.460	.....	.....	.....	.....	.....	2¾	2 <sup>11</sup> / <sub>16</sub>
0.470	.....	.....	.....	.....	.....	2 <sup>5</sup> / <sub>16</sub>	2¾
0.480	.....	.....	.....	.....	.....	2 <sup>5</sup> / <sub>16</sub>	2 <sup>11</sup> / <sub>16</sub>
0.490	.....	.....	.....	.....	.....	2¼	2¾
0.500	.....	.....	.....	.....	.....	2 <sup>3</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>
0.510	.....	.....	.....	.....	.....	.....	2½
0.520	.....	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>16</sub>
0.530	.....	.....	.....	.....	.....	.....	2¾
0.540	.....	.....	.....	.....	.....	.....	2 <sup>5</sup> / <sub>16</sub>
0.550	.....	.....	.....	.....	.....	.....	2 <sup>5</sup> / <sub>16</sub>
0.560	.....	.....	.....	.....	.....	.....	.....



TABLE 3-8 VALUES OF L FOR PIPE SIZES ≥ NPS 36 AND < NPS 42

Depth, d, in.	Wall Thickness, t, in.							
	0.250	0.281	0.312	0.375	0.406	0.469	0.562	0.688
0.030	13 <sup>7</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>4</sub>	.....	.....	.....	.....	.....	.....
0.040	13 <sup>7</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>4</sub>	15	16 <sup>7</sup> / <sub>16</sub>	.....	.....	.....	.....
0.050	9	13 <sup>7</sup> / <sub>16</sub>	15	16 <sup>7</sup> / <sub>16</sub>	17 <sup>1</sup> / <sub>8</sub>	18 <sup>7</sup> / <sub>16</sub>	.....	.....
0.060	6 <sup>1</sup> / <sub>4</sub>	8 <sup>1</sup> / <sub>4</sub>	11 <sup>1</sup> / <sub>8</sub>	16 <sup>7</sup> / <sub>16</sub>	17 <sup>1</sup> / <sub>8</sub>	18 <sup>7</sup> / <sub>16</sub>	20 <sup>1</sup> / <sub>8</sub>	.....
0.070	4 <sup>15</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	7 <sup>7</sup> / <sub>8</sub>	13 <sup>1</sup> / <sub>4</sub>	17 <sup>1</sup> / <sub>8</sub>	18 <sup>7</sup> / <sub>16</sub>	20 <sup>1</sup> / <sub>8</sub>	22 <sup>3</sup> / <sub>16</sub>
0.080	4 <sup>1</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	9 <sup>1</sup> / <sub>2</sub>	11 <sup>7</sup> / <sub>8</sub>	18 <sup>7</sup> / <sub>16</sub>	20 <sup>1</sup> / <sub>8</sub>	22 <sup>3</sup> / <sub>16</sub>
0.090	3 <sup>9</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>4</sub>	7 <sup>7</sup> / <sub>8</sub>	9 <sup>9</sup> / <sub>16</sub>	13 <sup>11</sup> / <sub>16</sub>	20 <sup>1</sup> / <sub>8</sub>	22 <sup>3</sup> / <sub>16</sub>
0.100	3 <sup>9</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>8</sub>	10 <sup>3</sup> / <sub>8</sub>	18 <sup>11</sup> / <sub>16</sub>	22 <sup>3</sup> / <sub>16</sub>
0.110	2 <sup>7</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>9</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>8</sub>	14 <sup>1</sup> / <sub>4</sub>	22 <sup>3</sup> / <sub>16</sub>
0.120	2 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	7 <sup>1</sup> / <sub>16</sub>	11 <sup>3</sup> / <sub>8</sub>	22 <sup>3</sup> / <sub>16</sub>
0.130	2 <sup>7</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	17 <sup>3</sup> / <sub>16</sub>
0.140	2 <sup>1</sup> / <sub>4</sub>	2 <sup>11</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>4</sub>	14 <sup>3</sup> / <sub>16</sub>
0.150	2 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>2</sub>	2 <sup>15</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	12 <sup>3</sup> / <sub>16</sub>
0.160	1 <sup>15</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>4</sub>	7 <sup>1</sup> / <sub>16</sub>	10 <sup>15</sup> / <sub>16</sub>
0.170	1 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>8</sub>	9 <sup>1</sup> / <sub>16</sub>
0.180	1 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	9
0.190	1 <sup>3</sup> / <sub>8</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>16</sub>
0.200	1 <sup>1</sup> / <sub>2</sub>	1 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>
0.210	.....	1 <sup>1</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>8</sub>	5 <sup>9</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>
0.220	.....	1 <sup>3</sup> / <sub>8</sub>	1 <sup>15</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>8</sub>	2 <sup>15</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>8</sub>
0.230	.....	.....	1 <sup>7</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>2</sub>	2 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>
0.240	.....	.....	1 <sup>1</sup> / <sub>4</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>
0.250	.....	.....	.....	2 <sup>1</sup> / <sub>4</sub>	2 <sup>9</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub>	5 <sup>7</sup> / <sub>8</sub>
0.260	.....	.....	.....	2 <sup>9</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>2</sub>	3 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>
0.270	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>8</sub>	3	3 <sup>15</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>
0.280	.....	.....	.....	2	2 <sup>5</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>16</sub>	5 <sup>9</sup> / <sub>16</sub>
0.290	.....	.....	.....	1 <sup>15</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	5
0.300	.....	.....	.....	1 <sup>7</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>8</sub>	2 <sup>11</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>16</sub>
0.310	.....	.....	.....	.....	2	2 <sup>9</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>
0.320	.....	.....	.....	.....	1 <sup>1</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>2</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>
0.330	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>
0.340	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>
0.350	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>4</sub>	3	4 <sup>3</sup> / <sub>8</sub>
0.360	.....	.....	.....	.....	.....	2 <sup>9</sup> / <sub>16</sub>	2 <sup>15</sup> / <sub>16</sub>	4
0.370	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>
0.380	.....	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>4</sub>
0.390	.....	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>
0.400	.....	.....	.....	.....	.....	.....	2 <sup>9</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>
0.410	.....	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>2</sub>	3 <sup>1</sup> / <sub>2</sub>
0.420	.....	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>
0.430	.....	.....	.....	.....	.....	.....	2 <sup>3</sup> / <sub>8</sub>	3 <sup>5</sup> / <sub>16</sub>
0.440	.....	.....	.....	.....	.....	.....	2 <sup>3</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>
0.450	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>8</sub>
0.460	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.470	.....	.....	.....	.....	.....	.....	.....	3
0.480	.....	.....	.....	.....	.....	.....	.....	2 <sup>15</sup> / <sub>16</sub>
0.490	.....	.....	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>8</sub>
0.500	.....	.....	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>
0.510	.....	.....	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>4</sub>
0.520	.....	.....	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>
0.530	.....	.....	.....	.....	.....	.....	.....	2 <sup>3</sup> / <sub>8</sub>
0.540	.....	.....	.....	.....	.....	.....	.....	2 <sup>9</sup> / <sub>16</sub>
0.550	.....	.....	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>2</sub>
0.560	.....	.....	.....	.....	.....	.....	.....	.....



Table 3-9

ASME B31G-1991

TABLE 3-9 VALUES OF L FOR PIPE SIZES ≥ NPS 42 AND < NPS 48

Depth, d, in.	Wall Thickness, t, in.								
	0.344	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.030	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.040	17	.....	.....	.....	.....	.....	.....	.....	.....
0.050	17	18½	19⅞	19¾	20½	.....	.....	.....	.....
0.060	17	18½	19⅞	19¾	20½	21¾	.....	.....	.....
0.070	10⅛	18½	19⅞	19¾	20½	21¾	22⅝	24⅞	.....
0.080	8⅞	12⅞	16⅞	19¾	20½	21¾	22⅝	24⅞	25⅞
0.090	6⅞	9⅞	12⅞	14⅞	18⅞	21¾	22⅝	24⅞	25⅞
0.100	5⅞	8⅞	9¾	11½	13¾	20⅞	22⅝	24⅞	25⅞
0.110	5¼	7⅞	8¾	9⅞	11½	15⅞	22⅞	24⅞	25⅞
0.120	4⅞	6⅞	7¼	8⅞	9½	12⅞	17⅞	24⅞	25⅞
0.130	4⅞	5⅞	6½	7⅞	8⅞	10¾	14	18¾	25⅞
0.140	4	5⅞	5⅞	6⅞	7½	9½	12⅞	15⅞	20¼
0.150	3⅞	4⅞	5⅞	6⅞	6⅞	8½	10⅞	13⅞	16⅞
0.160	3⅞	4⅞	5⅞	5⅞	6⅞	7¼	9⅞	11⅞	14⅞
0.170	3¼	4⅞	4⅞	5¼	5⅞	7⅞	8¾	10⅞	12⅞
0.180	3⅞	3⅞	4⅞	4⅞	5½	6⅞	8⅞	9⅞	11⅞
0.190	2⅞	3⅞	4⅞	4⅞	5⅞	6¼	7½	9	10⅞
0.200	2¾	3½	3⅞	4⅞	4⅞	5⅞	7⅞	8⅞	9⅞
0.210	2⅞	3⅞	3¾	4⅞	4⅞	5⅞	6⅞	7⅞	9⅞
0.220	2⅞	3⅞	3⅞	4	4⅞	5⅞	6⅞	7⅞	8⅞
0.230	2⅞	3⅞	3⅞	3⅞	4⅞	5⅞	6	7	8⅞
0.240	2¼	2⅞	3¼	3⅞	4	4⅞	5⅞	6⅞	7¾
0.250	2⅞	2⅞	3⅞	3½	3⅞	4⅞	5⅞	6⅞	7⅞
0.260	2⅞	2⅞	3	3⅞	3⅞	4⅞	5¼	6⅞	7
0.270	1⅞	2⅞	2⅞	3⅞	3⅞	4¼	5	5⅞	6⅞
0.280	.....	2⅞	2⅞	3⅞	3⅞	4⅞	4⅞	5⅞	6⅞
0.290	.....	2⅞	2⅞	3	3⅞	3⅞	4⅞	5⅞	6⅞
0.300	.....	2¼	2⅞	2⅞	3⅞	3⅞	4½	5⅞	6
0.310	.....	2⅞	2½	2¾	3⅞	3⅞	4⅞	5⅞	5¾
0.320	.....	2⅞	2⅞	2⅞	2⅞	3⅞	4⅞	4⅞	5⅞
0.330	.....	.....	2⅞	2⅞	2⅞	3⅞	4⅞	4⅞	5⅞
0.340	.....	.....	2¼	2½	2¾	3⅞	3⅞	4⅞	5¼
0.350	.....	.....	2⅞	2⅞	2⅞	3¼	3⅞	4⅞	5⅞
0.360	.....	.....	.....	2⅞	2⅞	3⅞	3⅞	4⅞	4⅞
0.370	.....	.....	.....	2¼	2½	3⅞	3⅞	4⅞	4¼
0.380	.....	.....	.....	.....	2⅞	2⅞	3½	4⅞	4⅞
0.390	.....	.....	.....	.....	2⅞	2⅞	3⅞	3⅞	4½
0.400	.....	.....	.....	.....	2⅞	2⅞	3⅞	3⅞	4⅞
0.410	.....	.....	.....	.....	.....	2¾	3¼	3¼	4⅞
0.420	.....	.....	.....	.....	.....	2⅞	3⅞	3⅞	4⅞
0.430	.....	.....	.....	.....	.....	2⅞	3⅞	3⅞	4⅞
0.440	.....	.....	.....	.....	.....	2½	3	3½	4
0.450	.....	.....	.....	.....	.....	.....	2⅞	3⅞	3⅞
0.460	.....	.....	.....	.....	.....	.....	2⅞	3⅞	3⅞
0.470	.....	.....	.....	.....	.....	.....	2¾	3¼	3¼
0.480	.....	.....	.....	.....	.....	.....	2⅞	3⅞	3⅞
0.490	.....	.....	.....	.....	.....	.....	2⅞	3⅞	3⅞
0.500	.....	.....	.....	.....	.....	.....	2⅞	3	3½
0.510	.....	.....	.....	.....	.....	.....	.....	2⅞	3⅞
0.520	.....	.....	.....	.....	.....	.....	.....	2⅞	3⅞

**TABLE 3-9 VALUES OF L FOR PIPE SIZES ≥ NPS 42 AND < NPS 48**

0.812	0.875	0.938	Wall Thickness, t, in.					1.250	Depth, d, in.
			1.000	1.062	1.125	1.188	1.250		
.....	.....	.....	.....	.....	.....	.....	.....	0.030	
.....	.....	.....	.....	.....	.....	.....	.....	0.040	
.....	.....	.....	.....	.....	.....	.....	.....	0.050	
.....	.....	.....	.....	.....	.....	.....	.....	0.060	
.....	.....	.....	.....	.....	.....	.....	.....	0.070	
.....	.....	.....	.....	.....	.....	.....	.....	0.080	
26 <sup>3</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	.....	0.090	
26 <sup>3</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	28 <sup>1</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	0.100	
26 <sup>3</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	28 <sup>1</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>	29 <sup>15</sup> / <sub>16</sub>	.....	.....	.....	0.110	
26 <sup>3</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	28 <sup>1</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>	29 <sup>15</sup> / <sub>16</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	.....	0.120	
26 <sup>3</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	28 <sup>1</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>	29 <sup>15</sup> / <sub>16</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.130	
26 <sup>3</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	28 <sup>1</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>	29 <sup>15</sup> / <sub>16</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.140	
21 <sup>1</sup> / <sub>4</sub>	27 <sup>3</sup> / <sub>16</sub>	28 <sup>1</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>	29 <sup>15</sup> / <sub>16</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.150	
18 <sup>3</sup> / <sub>16</sub>	23 <sup>3</sup> / <sub>16</sub>	28 <sup>1</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>	29 <sup>15</sup> / <sub>16</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.160	
15 <sup>3</sup> / <sub>4</sub>	19 <sup>9</sup> / <sub>16</sub>	24 <sup>13</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>	29 <sup>15</sup> / <sub>16</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.170	
14	17	20 <sup>15</sup> / <sub>16</sub>	26 <sup>1</sup> / <sub>4</sub>	29 <sup>15</sup> / <sub>16</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.180	
12 <sup>11</sup> / <sub>16</sub>	15 <sup>1</sup> / <sub>2</sub>	18 <sup>1</sup> / <sub>4</sub>	22 <sup>1</sup> / <sub>4</sub>	27 <sup>1</sup> / <sub>2</sub>	30 <sup>13</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.190	
11 <sup>1</sup> / <sub>2</sub>	13 <sup>11</sup> / <sub>16</sub>	16 <sup>1</sup> / <sub>4</sub>	19 <sup>7</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>2</sub>	29 <sup>1</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.200	
10 <sup>3</sup> / <sub>4</sub>	12 <sup>9</sup> / <sub>16</sub>	14 <sup>3</sup> / <sub>4</sub>	17 <sup>3</sup> / <sub>8</sub>	20 <sup>9</sup> / <sub>16</sub>	24 <sup>13</sup> / <sub>16</sub>	30 <sup>7</sup> / <sub>16</sub>	32 <sup>7</sup> / <sub>16</sub>	0.210	
10	11 <sup>1</sup> / <sub>2</sub>	13 <sup>3</sup> / <sub>16</sub>	15 <sup>3</sup> / <sub>4</sub>	18 <sup>7</sup> / <sub>16</sub>	21 <sup>13</sup> / <sub>16</sub>	26 <sup>1</sup> / <sub>2</sub>	31 <sup>3</sup> / <sub>4</sub>	0.220	
9 <sup>7</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>2</sub>	12 <sup>9</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>2</sub>	16 <sup>3</sup> / <sub>4</sub>	19 <sup>9</sup> / <sub>16</sub>	23	27 <sup>7</sup> / <sub>16</sub>	0.230	
8 <sup>1</sup> / <sub>2</sub>	10 <sup>1</sup> / <sub>4</sub>	11 <sup>1</sup> / <sub>4</sub>	13 <sup>7</sup> / <sub>16</sub>	15 <sup>7</sup> / <sub>16</sub>	17 <sup>13</sup> / <sub>16</sub>	20 <sup>1</sup> / <sub>16</sub>	24 <sup>1</sup> / <sub>2</sub>	0.240	
8 <sup>7</sup> / <sub>16</sub>	9 <sup>11</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>9</sup> / <sub>16</sub>	14 <sup>3</sup> / <sub>16</sub>	16 <sup>1</sup> / <sub>2</sub>	18 <sup>13</sup> / <sub>16</sub>	21 <sup>3</sup> / <sub>4</sub>	0.250	
8	9 <sup>9</sup> / <sub>16</sub>	10 <sup>7</sup> / <sub>16</sub>	11 <sup>13</sup> / <sub>16</sub>	13 <sup>3</sup> / <sub>8</sub>	15 <sup>1</sup> / <sub>4</sub>	17 <sup>3</sup> / <sub>8</sub>	19 <sup>13</sup> / <sub>16</sub>	0.260	
7 <sup>11</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>4</sub>	9 <sup>1</sup> / <sub>2</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>5</sup> / <sub>8</sub>	14 <sup>1</sup> / <sub>4</sub>	16 <sup>1</sup> / <sub>2</sub>	18 <sup>1</sup> / <sub>16</sub>	0.270	
7 <sup>1</sup> / <sub>2</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>7</sup> / <sub>16</sub>	10 <sup>5</sup> / <sub>8</sub>	11 <sup>15</sup> / <sub>16</sub>	13 <sup>7</sup> / <sub>16</sub>	15 <sup>1</sup> / <sub>2</sub>	17	0.280	
7 <sup>1</sup> / <sub>16</sub>	8	9	10 <sup>1</sup> / <sub>2</sub>	11 <sup>3</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>4</sub>	15 <sup>15</sup> / <sub>16</sub>	0.290	
6 <sup>13</sup> / <sub>16</sub>	7 <sup>11</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>2</sub>	9 <sup>11</sup> / <sub>16</sub>	10 <sup>13</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>16</sub>	13 <sup>1</sup> / <sub>2</sub>	15 <sup>1</sup> / <sub>16</sub>	0.300	
6 <sup>1</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>	10 <sup>5</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>2</sub>	12 <sup>13</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>4</sub>	0.310	
6 <sup>3</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>2</sub>	8	8 <sup>15</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	11	12 <sup>1</sup> / <sub>4</sub>	13 <sup>9</sup> / <sub>16</sub>	0.320	
6 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>11</sup> / <sub>16</sub>	8 <sup>9</sup> / <sub>16</sub>	9 <sup>9</sup> / <sub>16</sub>	10 <sup>9</sup> / <sub>16</sub>	11 <sup>11</sup> / <sub>16</sub>	12 <sup>15</sup> / <sub>16</sub>	0.330	
5 <sup>15</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>16</sub>	10 <sup>9</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>4</sub>	12 <sup>1</sup> / <sub>2</sub>	0.340	
5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	8	8 <sup>1</sup> / <sub>2</sub>	9 <sup>13</sup> / <sub>16</sub>	10 <sup>13</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>2</sub>	0.350	
5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	7	7 <sup>1</sup> / <sub>4</sub>	8 <sup>9</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	10 <sup>7</sup> / <sub>16</sub>	11 <sup>7</sup> / <sub>16</sub>	0.360	
5 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>1</sup> / <sub>2</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>2</sub>	10 <sup>1</sup> / <sub>16</sub>	11	0.370	
5 <sup>1</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>2</sub>	6 <sup>9</sup> / <sub>16</sub>	7 <sup>5</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>2</sub>	9 <sup>3</sup> / <sub>4</sub>	10 <sup>1</sup> / <sub>2</sub>	0.380	
5 <sup>1</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>8</sub>	7 <sup>1</sup> / <sub>16</sub>	7 <sup>13</sup> / <sub>16</sub>	8 <sup>9</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	10 <sup>5</sup> / <sub>16</sub>	0.390	
5	5 <sup>1</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>8</sub>	7 <sup>5</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>2</sub>	9 <sup>1</sup> / <sub>2</sub>	10	0.400	
4 <sup>7</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>2</sub>	8 <sup>1</sup> / <sub>2</sub>	9 <sup>11</sup> / <sub>16</sub>	0.410	
4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>2</sub>	8 <sup>1</sup> / <sub>2</sub>	9 <sup>1</sup> / <sub>2</sub>	0.420	
4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>8</sub>	7	7 <sup>11</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>8</sub>	9 <sup>1</sup> / <sub>2</sub>	0.430	
4 <sup>1</sup> / <sub>2</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>2</sub>	8 <sup>3</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>2</sub>	0.440	
4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>5</sup> / <sub>16</sub>	8	8 <sup>11</sup> / <sub>16</sub>	0.450	
4 <sup>3</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>13</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	0.460	
4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>8</sub>	7	7 <sup>5</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>4</sub>	0.470	
4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	0.480	
4	4 <sup>1</sup> / <sub>2</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>	7 <sup>1</sup> / <sub>8</sub>	0.490	
3 <sup>15</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	6	6 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>11</sup> / <sub>16</sub>	0.500	
3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6 <sup>3</sup> / <sub>8</sub>	6 <sup>15</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	0.510	
3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>8</sub>	0.520	

**TABLE 3-9 VALUES OF L FOR PIPE SIZES ≥ NPS 42 AND < NPS 48 (CONT'D)**

Depth, d, in.	Wall Thickness, t, in.								
	0.344	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.530	.....	.....	.....	.....	.....	.....	.....	2 <sup>13</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>
0.540	.....	.....	.....	.....	.....	.....	.....	2 <sup>3</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>16</sub>
0.550	.....	.....	.....	.....	.....	.....	.....	2 <sup>11</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>
0.560	.....	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.570	.....	.....	.....	.....	.....	.....	.....	.....	3
0.580	.....	.....	.....	.....	.....	.....	.....	.....	2 <sup>15</sup> / <sub>16</sub>
0.590	.....	.....	.....	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>8</sub>
0.600	.....	.....	.....	.....	.....	.....	.....	.....	2 <sup>13</sup> / <sub>16</sub>
0.610	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.620	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.630	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.640	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.650	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.660	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.670	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.680	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.690	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.700	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.710	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.720	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.730	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.740	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.750	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.760	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.770	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.780	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.790	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.800	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.810	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.820	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.830	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.840	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.850	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.860	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.870	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.880	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.890	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.900	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.910	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.920	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.930	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.940	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.950	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.960	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.970	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.980	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.990	.....	.....	.....	.....	.....	.....	.....	.....	.....
1.000	.....	.....	.....	.....	.....	.....	.....	.....	.....
1.010	.....	.....	.....	.....	.....	.....	.....	.....	.....

**TABLE 3-9 VALUES OF L FOR PIPE SIZES ≥ NPS 42 AND < NPS 48 (CONT'D)**

0.812	0.875	0.938	Wall Thickness, t, in.					Depth, d, in.
			1.000	1.062	1.125	1.188	1.250	
3 <sup>11</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>	0.530
3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>3</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>8</sub>	0.540
3 <sup>7</sup> / <sub>16</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	6 <sup>15</sup> / <sub>16</sub>	0.550
3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	0.560
3 <sup>7</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	6 <sup>11</sup> / <sub>16</sub>	0.570
3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>9</sup> / <sub>16</sub>	0.580
3 <sup>5</sup> / <sub>16</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>3</sup> / <sub>16</sub>	0.590
3 <sup>1</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>8</sub>	0.600
3 <sup>3</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>4</sub>	0.610
3 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	0.620
3 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	0.630
3	3 <sup>3</sup> / <sub>8</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	5 <sup>15</sup> / <sub>16</sub>	0.640
.....	3 <sup>5</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>13</sup> / <sub>16</sub>	0.650
.....	3 <sup>1</sup> / <sub>4</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	0.660
.....	3 <sup>3</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>8</sub>	4	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>11</sup> / <sub>16</sub>	0.670
.....	3 <sup>1</sup> / <sub>8</sub>	3 <sup>9</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>9</sup> / <sub>16</sub>	0.680
.....	3 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	0.690
.....	3 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>7</sup> / <sub>16</sub>	0.700
.....	.....	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	0.710
.....	.....	3 <sup>5</sup> / <sub>16</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>4</sub>	0.720
.....	.....	3 <sup>1</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>8</sub>	4	4 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>16</sub>	0.730
.....	.....	3 <sup>3</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	0.740
.....	.....	3 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>5</sup> / <sub>8</sub>	5	0.750
.....	.....	.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	0.760
.....	.....	.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>7</sup> / <sub>8</sub>	0.770
.....	.....	.....	3 <sup>1</sup> / <sub>8</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	0.780
.....	.....	.....	3 <sup>3</sup> / <sub>16</sub>	3 <sup>11</sup> / <sub>16</sub>	4	4 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>	0.790
.....	.....	.....	3 <sup>1</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>8</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	0.800
.....	.....	.....	.....	3 <sup>9</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>8</sub>	0.810
.....	.....	.....	.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	0.820
.....	.....	.....	.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	0.830
.....	.....	.....	.....	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>16</sub>	0.840
.....	.....	.....	.....	.....	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	0.850
.....	.....	.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	4	4 <sup>3</sup> / <sub>16</sub>	0.860
.....	.....	.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	0.870
.....	.....	.....	.....	.....	3 <sup>9</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	0.880
.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	0.890
.....	.....	.....	.....	.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	0.900
.....	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>16</sub>	0.910
.....	.....	.....	.....	.....	.....	3 <sup>11</sup> / <sub>16</sub>	4	0.920
.....	.....	.....	.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	3 <sup>15</sup> / <sub>16</sub>	0.930
.....	.....	.....	.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	3 <sup>15</sup> / <sub>16</sub>	0.940
.....	.....	.....	.....	.....	.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	0.950
.....	.....	.....	.....	.....	.....	.....	3 <sup>13</sup> / <sub>16</sub>	0.960
.....	.....	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>4</sub>	0.970
.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>4</sub>	0.980
.....	.....	.....	.....	.....	.....	.....	3 <sup>11</sup> / <sub>16</sub>	0.990
.....	.....	.....	.....	.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	1.000
.....	.....	.....	.....	.....	.....	.....	.....	1.010

**TABLE 3-10 VALUES OF L FOR PIPE SIZES ≥ NPS 48 AND < NPS 52**

Depth, d, in.	Wall Thickness, t, in.								
	0.344	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.030	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.040	18 <sup>3</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	.....	.....	.....
0.050	18 <sup>3</sup> / <sub>16</sub>	19 <sup>3</sup> / <sub>4</sub>	20 <sup>3</sup> / <sub>16</sub>	21 <sup>1</sup> / <sub>4</sub>	21 <sup>15</sup> / <sub>16</sub>	.....	.....	.....	.....
0.060	18 <sup>3</sup> / <sub>16</sub>	19 <sup>3</sup> / <sub>4</sub>	20 <sup>3</sup> / <sub>16</sub>	21 <sup>1</sup> / <sub>4</sub>	21 <sup>15</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>4</sub>	.....	.....	.....
0.070	11 <sup>1</sup> / <sub>16</sub>	19 <sup>3</sup> / <sub>4</sub>	20 <sup>3</sup> / <sub>16</sub>	21 <sup>1</sup> / <sub>4</sub>	21 <sup>15</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>4</sub>	24 <sup>3</sup> / <sub>16</sub>	25 <sup>1</sup> / <sub>4</sub>	.....
0.080	8 <sup>1</sup> / <sub>16</sub>	13 <sup>3</sup> / <sub>4</sub>	17 <sup>1</sup> / <sub>16</sub>	21 <sup>1</sup> / <sub>4</sub>	21 <sup>15</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>4</sub>	24 <sup>3</sup> / <sub>16</sub>	25 <sup>3</sup> / <sub>4</sub>	26 <sup>3</sup> / <sub>16</sub>
0.090	7 <sup>3</sup> / <sub>8</sub>	10 <sup>3</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>8</sub>	15 <sup>13</sup> / <sub>16</sub>	19 <sup>13</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>4</sub>	24 <sup>3</sup> / <sub>16</sub>	25 <sup>3</sup> / <sub>4</sub>	26 <sup>3</sup> / <sub>16</sub>
0.100	6 <sup>5</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>4</sub>	10 <sup>3</sup> / <sub>8</sub>	12 <sup>5</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>16</sub>	21 <sup>7</sup> / <sub>8</sub>	24 <sup>3</sup> / <sub>16</sub>	25 <sup>3</sup> / <sub>4</sub>	26 <sup>3</sup> / <sub>16</sub>
0.110	5 <sup>3</sup> / <sub>8</sub>	7 <sup>5</sup> / <sub>16</sub>	8 <sup>13</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>4</sub>	11 <sup>1</sup> / <sub>16</sub>	16 <sup>7</sup> / <sub>16</sub>	24	25 <sup>3</sup> / <sub>4</sub>	26 <sup>3</sup> / <sub>16</sub>
0.120	5 <sup>1</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>3</sup> / <sub>4</sub>	8 <sup>3</sup> / <sub>8</sub>	10 <sup>3</sup> / <sub>16</sub>	13 <sup>7</sup> / <sub>16</sub>	18 <sup>1</sup> / <sub>4</sub>	25 <sup>3</sup> / <sub>4</sub>	26 <sup>3</sup> / <sub>16</sub>
0.130	4 <sup>3</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>15</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>5</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>2</sub>	15	20	26 <sup>3</sup> / <sub>16</sub>
0.140	4 <sup>1</sup> / <sub>4</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8	10 <sup>3</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>8</sub>	16 <sup>1</sup> / <sub>2</sub>	21 <sup>3</sup> / <sub>8</sub>
0.150	3 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>8</sub>	11 <sup>3</sup> / <sub>8</sub>	14 <sup>1</sup> / <sub>4</sub>	18
0.160	3 <sup>11</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	8 <sup>5</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>4</sub>	12 <sup>3</sup> / <sub>8</sub>	15 <sup>5</sup> / <sub>16</sub>
0.170	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>4</sub>	7 <sup>1</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>8</sub>	11 <sup>3</sup> / <sub>8</sub>	13 <sup>13</sup> / <sub>16</sub>
0.180	3 <sup>1</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	7 <sup>1</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>8</sub>	10 <sup>3</sup> / <sub>8</sub>	12 <sup>7</sup> / <sub>16</sub>
0.190	3 <sup>1</sup> / <sub>16</sub>	4	4 <sup>1</sup> / <sub>2</sub>	5	5 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>8</sub>	11 <sup>3</sup> / <sub>8</sub>
0.200	2 <sup>15</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	8 <sup>15</sup> / <sub>16</sub>	10 <sup>3</sup> / <sub>16</sub>
0.210	2 <sup>1</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>16</sub>	4	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>3</sup> / <sub>8</sub>	9 <sup>13</sup> / <sub>16</sub>
0.220	2 <sup>3</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>15</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>
0.230	2 <sup>1</sup> / <sub>2</sub>	3 <sup>1</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>8</sub>	7 <sup>1</sup> / <sub>2</sub>	8 <sup>1</sup> / <sub>16</sub>
0.240	2 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>4</sub>
0.250	2 <sup>5</sup> / <sub>16</sub>	3	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>
0.260	2 <sup>3</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>2</sub>
0.270	2 <sup>1</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>4</sub>	7 <sup>1</sup> / <sub>16</sub>
0.280	.....	2 <sup>5</sup> / <sub>16</sub>	3	3 <sup>5</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	6	6 <sup>3</sup> / <sub>8</sub>
0.290	.....	2 <sup>9</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>4</sub>	5	5 <sup>3</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>8</sub>
0.300	.....	2 <sup>7</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>8</sub>
0.310	.....	2 <sup>3</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	2 <sup>15</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>16</sub>
0.320	.....	2 <sup>1</sup> / <sub>4</sub>	2 <sup>9</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>
0.330	.....	.....	2 <sup>1</sup> / <sub>2</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>
0.340	.....	.....	2 <sup>3</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>16</sub>	3	3 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>
0.350	.....	.....	2 <sup>5</sup> / <sub>16</sub>	2 <sup>9</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>5</sup> / <sub>16</sub>
0.360	.....	.....	.....	2 <sup>1</sup> / <sub>2</sub>	2 <sup>13</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4	4 <sup>3</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>4</sub>
0.370	.....	.....	.....	2 <sup>7</sup> / <sub>16</sub>	2 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>3</sup> / <sub>8</sub>
0.380	.....	.....	.....	.....	2 <sup>5</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>8</sub>	5
0.390	.....	.....	.....	.....	2 <sup>9</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>13</sup> / <sub>16</sub>
0.400	.....	.....	.....	.....	2 <sup>7</sup> / <sub>16</sub>	3	3 <sup>5</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>
0.410	.....	.....	.....	.....	.....	2 <sup>15</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	4	4 <sup>5</sup> / <sub>16</sub>
0.420	.....	.....	.....	.....	.....	2 <sup>13</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>
0.430	.....	.....	.....	.....	.....	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>4</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>
0.440	.....	.....	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub>
0.450	.....	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>16</sub>
0.460	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>
0.470	.....	.....	.....	.....	.....	.....	2 <sup>15</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	4
0.480	.....	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>
0.490	.....	.....	.....	.....	.....	.....	2 <sup>13</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>
0.500	.....	.....	.....	.....	.....	.....	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>
0.510	.....	.....	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>
0.520	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>

**TABLE 3-10 VALUES OF L FOR PIPE SIZES ≥ NPS 48 AND < NPS 52**

0.812	0.875	0.938	Wall Thickness, t, in.					Depth, d, in.
			1.000	1.062	1.125	1.188	1.250	
.....	.....	.....	.....	.....	.....	.....	.....	0.030
.....	.....	.....	.....	.....	.....	.....	.....	0.040
.....	.....	.....	.....	.....	.....	.....	.....	0.050
.....	.....	.....	.....	.....	.....	.....	.....	0.060
.....	.....	.....	.....	.....	.....	.....	.....	0.070
.....	.....	.....	.....	.....	.....	.....	.....	0.080
28	29 <sup>1</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	.....	0.090
28	29 <sup>1</sup> / <sub>16</sub>	30 <sup>1</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	0.100
28	29 <sup>1</sup> / <sub>16</sub>	30 <sup>1</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32	.....	.....	.....	0.110
28	29 <sup>1</sup> / <sub>16</sub>	30 <sup>1</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	.....	0.120
28	29 <sup>1</sup> / <sub>16</sub>	30 <sup>1</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.130
28	29 <sup>1</sup> / <sub>16</sub>	30 <sup>1</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.140
23 <sup>3</sup> / <sub>4</sub>	29 <sup>1</sup> / <sub>16</sub>	30 <sup>1</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.150
19 <sup>7</sup> / <sub>16</sub>	24 <sup>15</sup> / <sub>16</sub>	30 <sup>1</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.160
16 <sup>13</sup> / <sub>16</sub>	20 <sup>15</sup> / <sub>16</sub>	26 <sup>3</sup> / <sub>16</sub>	31 <sup>1</sup> / <sub>16</sub>	32	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.170
14 <sup>15</sup> / <sub>16</sub>	18 <sup>3</sup> / <sub>16</sub>	22 <sup>3</sup> / <sub>8</sub>	28 <sup>1</sup> / <sub>16</sub>	32	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.180
13 <sup>3</sup> / <sub>16</sub>	16 <sup>3</sup> / <sub>16</sub>	19 <sup>1</sup> / <sub>2</sub>	23 <sup>3</sup> / <sub>4</sub>	29 <sup>1</sup> / <sub>2</sub>	32 <sup>15</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.190
12 <sup>3</sup> / <sub>8</sub>	14 <sup>1</sup> / <sub>16</sub>	17 <sup>3</sup> / <sub>8</sub>	20 <sup>3</sup> / <sub>4</sub>	25 <sup>1</sup> / <sub>8</sub>	31 <sup>1</sup> / <sub>16</sub>	33 <sup>13</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.200
11 <sup>1</sup> / <sub>2</sub>	13 <sup>7</sup> / <sub>16</sub>	15 <sup>3</sup> / <sub>4</sub>	18 <sup>1</sup> / <sub>16</sub>	22	26 <sup>1</sup> / <sub>2</sub>	32 <sup>3</sup> / <sub>16</sub>	34 <sup>11</sup> / <sub>16</sub>	0.210
10 <sup>3</sup> / <sub>4</sub>	12 <sup>7</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>2</sub>	16 <sup>3</sup> / <sub>8</sub>	19 <sup>1</sup> / <sub>16</sub>	23 <sup>3</sup> / <sub>16</sub>	27 <sup>15</sup> / <sub>16</sub>	33 <sup>15</sup> / <sub>16</sub>	0.220
10 <sup>1</sup> / <sub>16</sub>	11 <sup>5</sup> / <sub>8</sub>	13 <sup>7</sup> / <sub>16</sub>	15 <sup>1</sup> / <sub>2</sub>	17 <sup>15</sup> / <sub>16</sub>	20 <sup>15</sup> / <sub>16</sub>	24 <sup>3</sup> / <sub>16</sub>	29 <sup>9</sup> / <sub>16</sub>	0.230
9 <sup>1</sup> / <sub>2</sub>	10 <sup>15</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>16</sub>	14 <sup>3</sup> / <sub>8</sub>	16 <sup>1</sup> / <sub>2</sub>	19 <sup>1</sup> / <sub>16</sub>	22 <sup>1</sup> / <sub>8</sub>	25 <sup>13</sup> / <sub>16</sub>	0.240
9	10 <sup>5</sup> / <sub>16</sub>	11 <sup>13</sup> / <sub>16</sub>	13 <sup>3</sup> / <sub>16</sub>	15 <sup>5</sup> / <sub>16</sub>	17 <sup>1</sup> / <sub>2</sub>	20 <sup>1</sup> / <sub>8</sub>	23 <sup>3</sup> / <sub>4</sub>	0.250
8 <sup>3</sup> / <sub>16</sub>	9 <sup>13</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>8</sub>	12 <sup>5</sup> / <sub>8</sub>	14 <sup>3</sup> / <sub>16</sub>	16 <sup>5</sup> / <sub>16</sub>	18 <sup>1</sup> / <sub>16</sub>	21 <sup>3</sup> / <sub>16</sub>	0.260
8 <sup>1</sup> / <sub>16</sub>	9 <sup>5</sup> / <sub>16</sub>	10 <sup>9</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>16</sub>	13 <sup>1</sup> / <sub>2</sub>	15 <sup>1</sup> / <sub>4</sub>	17 <sup>1</sup> / <sub>4</sub>	19 <sup>9</sup> / <sub>16</sub>	0.270
7 <sup>7</sup> / <sub>8</sub>	8 <sup>15</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>16</sub>	11 <sup>3</sup> / <sub>8</sub>	12 <sup>3</sup> / <sub>4</sub>	14 <sup>3</sup> / <sub>8</sub>	16 <sup>3</sup> / <sub>16</sub>	18 <sup>3</sup> / <sub>16</sub>	0.280
7 <sup>1</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>	9 <sup>5</sup> / <sub>8</sub>	10 <sup>13</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>8</sub>	13 <sup>3</sup> / <sub>16</sub>	15 <sup>1</sup> / <sub>4</sub>	17 <sup>1</sup> / <sub>16</sub>	0.290
7 <sup>1</sup> / <sub>4</sub>	8 <sup>3</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>	10 <sup>3</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>15</sup> / <sub>16</sub>	14 <sup>7</sup> / <sub>16</sub>	16 <sup>1</sup> / <sub>16</sub>	0.300
7	7 <sup>7</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>8</sub>	9 <sup>5</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>5</sup> / <sub>16</sub>	13 <sup>11</sup> / <sub>16</sub>	15 <sup>1</sup> / <sub>4</sub>	0.310
6 <sup>3</sup> / <sub>4</sub>	7 <sup>5</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>9</sup> / <sub>16</sub>	10 <sup>5</sup> / <sub>8</sub>	11 <sup>13</sup> / <sub>16</sub>	13 <sup>1</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>2</sub>	0.320
6 <sup>1</sup> / <sub>2</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>4</sub>	9 <sup>3</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>2</sub>	13 <sup>13</sup> / <sub>16</sub>	0.330
6 <sup>5</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>15</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>8</sub>	9 <sup>13</sup> / <sub>16</sub>	10 <sup>7</sup> / <sub>8</sub>	12	13 <sup>3</sup> / <sub>4</sub>	0.340
6 <sup>1</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>8</sub>	7 <sup>11</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>2</sub>	10 <sup>1</sup> / <sub>2</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>11</sup> / <sub>16</sub>	0.350
5 <sup>15</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>2</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>8</sub>	11 <sup>1</sup> / <sub>8</sub>	12 <sup>3</sup> / <sub>16</sub>	0.360
5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>4</sub>	8 <sup>1</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>8</sub>	9 <sup>3</sup> / <sub>4</sub>	10 <sup>3</sup> / <sub>4</sub>	11 <sup>3</sup> / <sub>4</sub>	0.370
5 <sup>5</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	7 <sup>13</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>8</sub>	9 <sup>1</sup> / <sub>2</sub>	10 <sup>3</sup> / <sub>8</sub>	11 <sup>3</sup> / <sub>8</sub>	0.380
5 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>8</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>8</sub>	9 <sup>1</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>16</sub>	11	0.390
5 <sup>5</sup> / <sub>16</sub>	6	6 <sup>11</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>8</sub>	8 <sup>15</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>4</sub>	10 <sup>11</sup> / <sub>16</sub>	0.400
5 <sup>3</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>3</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>8</sub>	8 <sup>11</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>2</sub>	10 <sup>5</sup> / <sub>16</sub>	0.410
5 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7	7 <sup>11</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>	10 <sup>1</sup> / <sub>16</sub>	0.420
4 <sup>15</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>2</sub>	8 <sup>1</sup> / <sub>4</sub>	9	9 <sup>3</sup> / <sub>4</sub>	0.430
4 <sup>13</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	6	6 <sup>5</sup> / <sub>8</sub>	7 <sup>5</sup> / <sub>16</sub>	8	8 <sup>3</sup> / <sub>4</sub>	9 <sup>1</sup> / <sub>2</sub>	0.440
4 <sup>11</sup> / <sub>16</sub>	5 <sup>9</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>13</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>	0.450
4 <sup>3</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>8</sub>	7	7 <sup>5</sup> / <sub>8</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	0.460
4 <sup>1</sup> / <sub>2</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>8</sub>	8 <sup>13</sup> / <sub>16</sub>	0.470
4 <sup>3</sup> / <sub>8</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	7 <sup>15</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>8</sub>	0.480
4 <sup>3</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>4</sub>	8 <sup>7</sup> / <sub>16</sub>	0.490
4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>8</sub>	7	7 <sup>5</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>4</sub>	0.500
4 <sup>1</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	0.510
4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>5</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>8</sub>	0.520



**TABLE 3-10 VALUES OF L FOR PIPE SIZES ≥ NPS 48 AND < NPS 52 (CONT'D)**

Depth, d, in.	Wall Thickness, t, in.								
	0.344	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.530	.....	.....	.....	.....	.....	.....	.....	3	3½
0.540	.....	.....	.....	.....	.....	.....	.....	2 <sup>15</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>
0.550	.....	.....	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>
0.560	.....	.....	.....	.....	.....	.....	.....	.....	3¼
0.570	.....	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.580	.....	.....	.....	.....	.....	.....	.....	.....	3½
0.590	.....	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.600	.....	.....	.....	.....	.....	.....	.....	.....	3
0.610	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.620	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.630	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.640	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.650	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.660	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.670	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.680	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.690	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.700	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.710	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.720	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.730	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.740	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.750	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.760	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.770	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.780	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.790	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.800	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.810	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.820	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.830	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.840	.....	.....	.....	.....	.....	.....	.....	.....	.....
0.850	.....	.....	.....	.....	.....	.....	.....	.....	.....

**TABLE 3-10 VALUES OF L FOR PIPE SIZES ≥ NPS 48 AND < NPS 52 (CONT'D)**

0.812	0.875	0.938	Wall Thickness, t, in.					Depth, d, in.
			1.000	1.062	1.125	1.188	1.250	
3 <sup>15</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>9</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>4</sub>	0.530
3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>16</sub>	7	7 <sup>9</sup> / <sub>16</sub>	0.540
3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>8</sub>	7 <sup>1</sup> / <sub>16</sub>	0.550
3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>5</sup> / <sub>16</sub>	0.560
3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>16</sub>	0.570
3 <sup>9</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	5	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>16</sub>	0.580
3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>8</sub>	6 <sup>15</sup> / <sub>16</sub>	0.590
3 <sup>7</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>13</sup> / <sub>16</sub>	0.600
3 <sup>5</sup> / <sub>8</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	6 <sup>11</sup> / <sub>16</sub>	0.610
3 <sup>5</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>9</sup> / <sub>16</sub>	0.620
3 <sup>1</sup> / <sub>4</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>1</sup> / <sub>2</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	0.630
3 <sup>3</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>8</sub>	0.640
.....	3 <sup>3</sup> / <sub>16</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>4</sub>	0.650
.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	0.660
.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>16</sub>	0.670
.....	3 <sup>3</sup> / <sub>8</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	.....	.....	.....	0.680
.....	3 <sup>5</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	.....	.....	.....	0.690
.....	3 <sup>1</sup> / <sub>4</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	.....	.....	.....	0.700
.....	.....	3 <sup>5</sup> / <sub>8</sub>	4	4 <sup>7</sup> / <sub>16</sub>	.....	.....	.....	0.710
.....	.....	3 <sup>9</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	.....	.....	.....	0.720
.....	.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	.....	.....	.....	0.730
.....	.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	.....	.....	.....	0.740
.....	.....	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	.....	.....	.....	0.750
.....	.....	.....	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	.....	.....	.....	0.760
.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	4	.....	.....	.....	0.770
.....	.....	.....	3 <sup>9</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	.....	.....	.....	0.780
.....	.....	.....	3 <sup>11</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	.....	.....	.....	0.790
.....	.....	.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>7</sup> / <sub>8</sub>	.....	.....	.....	0.800
.....	.....	.....	.....	3 <sup>13</sup> / <sub>16</sub>	.....	.....	.....	0.810
.....	.....	.....	.....	3 <sup>3</sup> / <sub>4</sub>	.....	.....	.....	0.820
.....	.....	.....	.....	3 <sup>11</sup> / <sub>16</sub>	.....	.....	.....	0.830
.....	.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	.....	.....	.....	0.840
.....	.....	.....	.....	.....	.....	.....	.....	0.850

**TABLE 3-11 VALUES OF L FOR PIPE SIZES ≥ NPS 52 AND < NPS 56**

Depth, d, in.	Wall Thickness, t, in.							
	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.040	.....	.....	.....	.....	.....	.....	.....	.....
0.050	20 <sup>9</sup> / <sub>16</sub>	21 <sup>3</sup> / <sub>16</sub>	22 <sup>1</sup> / <sub>16</sub>	22 <sup>13</sup> / <sub>16</sub>	.....	.....	.....	.....
0.060	20 <sup>9</sup> / <sub>16</sub>	21 <sup>3</sup> / <sub>16</sub>	22 <sup>1</sup> / <sub>16</sub>	22 <sup>13</sup> / <sub>16</sub>	24 <sup>3</sup> / <sub>16</sub>	.....	.....	.....
0.070	20 <sup>9</sup> / <sub>16</sub>	21 <sup>3</sup> / <sub>16</sub>	22 <sup>1</sup> / <sub>16</sub>	22 <sup>13</sup> / <sub>16</sub>	24 <sup>3</sup> / <sub>16</sub>	25 <sup>5</sup> / <sub>16</sub>	26 <sup>13</sup> / <sub>16</sub>	.....
0.080	14 <sup>7</sup> / <sub>16</sub>	18 <sup>7</sup> / <sub>16</sub>	22 <sup>1</sup> / <sub>16</sub>	22 <sup>13</sup> / <sub>16</sub>	24 <sup>3</sup> / <sub>16</sub>	25 <sup>5</sup> / <sub>16</sub>	26 <sup>13</sup> / <sub>16</sub>	28
0.090	11	13 <sup>7</sup> / <sub>16</sub>	16 <sup>1</sup> / <sub>2</sub>	20 <sup>5</sup> / <sub>16</sub>	24 <sup>3</sup> / <sub>16</sub>	25 <sup>5</sup> / <sub>16</sub>	26 <sup>13</sup> / <sub>16</sub>	28
0.100	9 <sup>1</sup> / <sub>16</sub>	10 <sup>13</sup> / <sub>16</sub>	12 <sup>13</sup> / <sub>16</sub>	15 <sup>5</sup> / <sub>16</sub>	22 <sup>3</sup> / <sub>4</sub>	25 <sup>5</sup> / <sub>16</sub>	26 <sup>13</sup> / <sub>16</sub>	28
0.110	7 <sup>7</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>16</sub>	10 <sup>11</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>8</sub>	17 <sup>1</sup> / <sub>8</sub>	25	26 <sup>13</sup> / <sub>16</sub>	28
0.120	7	8 <sup>1</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>	10 <sup>9</sup> / <sub>16</sub>	14	19	26 <sup>13</sup> / <sub>16</sub>	28
0.130	6 <sup>5</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>	8 <sup>3</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	11 <sup>15</sup> / <sub>16</sub>	15 <sup>5</sup> / <sub>16</sub>	20 <sup>13</sup> / <sub>16</sub>	28
0.140	5 <sup>3</sup> / <sub>4</sub>	6 <sup>9</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>8</sub>	10 <sup>9</sup> / <sub>16</sub>	13 <sup>3</sup> / <sub>8</sub>	17 <sup>3</sup> / <sub>16</sub>	22 <sup>9</sup> / <sub>16</sub>
0.150	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>5</sup> / <sub>8</sub>	9 <sup>1</sup> / <sub>2</sub>	11 <sup>13</sup> / <sub>16</sub>	14 <sup>13</sup> / <sub>16</sub>	18 <sup>3</sup> / <sub>4</sub>
0.160	5	5 <sup>5</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>16</sub>	7	8 <sup>11</sup> / <sub>16</sub>	10 <sup>5</sup> / <sub>8</sub>	13 <sup>1</sup> / <sub>8</sub>	16 <sup>5</sup> / <sub>16</sub>
0.170	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>2</sub>	8	9 <sup>3</sup> / <sub>4</sub>	11 <sup>13</sup> / <sub>16</sub>	14 <sup>3</sup> / <sub>8</sub>
0.180	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>8</sub>	7 <sup>7</sup> / <sub>16</sub>	9	10 <sup>13</sup> / <sub>16</sub>	12 <sup>15</sup> / <sub>16</sub>
0.190	4 <sup>1</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>15</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>8</sub>	10	11 <sup>7</sup> / <sub>8</sub>
0.200	3 <sup>15</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>16</sub>	6 <sup>9</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>8</sub>	9 <sup>5</sup> / <sub>16</sub>	11
0.210	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>3</sup> / <sub>4</sub>	10 <sup>1</sup> / <sub>4</sub>
0.220	3 <sup>3</sup> / <sub>16</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	7	8 <sup>1</sup> / <sub>4</sub>	9 <sup>5</sup> / <sub>8</sub>
0.230	3 <sup>3</sup> / <sub>8</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>8</sub>	7 <sup>13</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>
0.240	3 <sup>1</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>3</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>8</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>9</sup> / <sub>16</sub>
0.250	3 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>
0.260	3	3 <sup>3</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>13</sup> / <sub>16</sub>
0.270	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>2</sub>
0.280	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>4</sub>	7 <sup>3</sup> / <sub>16</sub>
0.290	2 <sup>5</sup> / <sub>8</sub>	3	3 <sup>5</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	6	6 <sup>7</sup> / <sub>8</sub>
0.300	2 <sup>5</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	5	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>8</sub>
0.310	2 <sup>7</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>16</sub>
0.320	2 <sup>5</sup> / <sub>8</sub>	2 <sup>11</sup> / <sub>16</sub>	3	3 <sup>3</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>
0.330	.....	2 <sup>9</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>1</sup> / <sub>4</sub>	6
0.340	.....	2 <sup>1</sup> / <sub>2</sub>	2 <sup>13</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>
0.350	.....	2 <sup>3</sup> / <sub>8</sub>	2 <sup>11</sup> / <sub>16</sub>	3	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>
0.360	.....	.....	2 <sup>5</sup> / <sub>8</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>
0.370	.....	.....	2 <sup>1</sup> / <sub>2</sub>	2 <sup>13</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>8</sub>	4	4 <sup>11</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>
0.380	.....	.....	.....	2 <sup>3</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	5 <sup>3</sup> / <sub>16</sub>
0.390	.....	.....	.....	2 <sup>5</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>
0.400	.....	.....	.....	2 <sup>5</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>8</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>
0.410	.....	.....	.....	.....	3	3 <sup>5</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>
0.420	.....	.....	.....	.....	2 <sup>15</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>
0.430	.....	.....	.....	.....	2 <sup>7</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	4	4 <sup>9</sup> / <sub>16</sub>
0.440	.....	.....	.....	.....	2 <sup>13</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>16</sub>
0.450	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>4</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>
0.460	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>16</sub>	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>
0.470	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>8</sub>
0.480	.....	.....	.....	.....	.....	3	3 <sup>1</sup> / <sub>2</sub>	4 <sup>1</sup> / <sub>16</sub>
0.490	.....	.....	.....	.....	.....	2 <sup>15</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>
0.500	.....	.....	.....	.....	.....	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>8</sub>
0.510	.....	.....	.....	.....	.....	.....	3 <sup>5</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>
0.520	.....	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>16</sub>	3 <sup>11</sup> / <sub>16</sub>
0.530	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>8</sub>	3 <sup>5</sup> / <sub>8</sub>



**TABLE 3-11 VALUES OF L FOR PIPE SIZES ≥ NPS 52 AND < NPS 56**

0.812	0.875	0.938	Wall Thickness, t, in.				1.125	1.188	1.250	Depth, d, in.
			1.000	1.062	1.125	1.188				
.....	.....	.....	.....	.....	.....	.....	.....	.....	0.040	
.....	.....	.....	.....	.....	.....	.....	.....	.....	0.050	
.....	.....	.....	.....	.....	.....	.....	.....	.....	0.060	
.....	.....	.....	.....	.....	.....	.....	.....	.....	0.070	
.....	.....	.....	.....	.....	.....	.....	.....	.....	0.080	
29 1/8	30 1/4	.....	.....	.....	.....	.....	.....	.....	0.090	
29 1/8	30 1/4	31 1/16	.....	.....	.....	.....	.....	.....	0.100	
29 1/8	30 1/4	31 1/16	32 5/16	33 3/16	.....	.....	.....	.....	0.110	
29 1/8	30 1/4	31 1/16	32 5/16	33 3/16	34 1/4	35 3/16	.....	.....	0.120	
29 1/8	30 1/4	31 1/16	32 5/16	33 3/16	34 1/4	35 3/16	36 1/8	.....	0.130	
29 1/8	30 1/4	31 1/16	32 5/16	33 3/16	34 1/4	35 3/16	36 1/8	.....	0.140	
24 3/16	30 1/4	31 1/16	32 5/16	33 3/16	34 1/4	35 3/16	36 1/8	.....	0.150	
20 3/16	25 15/16	31 1/16	32 5/16	33 3/16	34 1/4	35 3/16	36 1/8	.....	0.160	
17 1/2	21 1/4	27 3/8	32 5/16	33 3/16	34 1/4	35 3/16	36 1/8	.....	0.170	
15 5/16	18 15/16	23 3/16	29 3/16	33 3/16	34 1/4	35 3/16	36 1/8	.....	0.180	
14 1/16	16 7/8	20 3/16	24 3/4	30 1 1/16	34 1/4	35 3/16	36 1/8	.....	0.190	
12 15/16	15 1/4	18 1/8	21 5/8	26 1/8	32 5/16	35 3/16	36 1/8	.....	0.200	
11 15/16	14	16 7/16	19 5/16	22 15/16	27 3/8	33 3/8	36 1/8	.....	0.210	
11 3/16	12 15/16	15 1/16	17 7/16	20 1/2	24 1/4	29 1/16	35 3/16	.....	0.220	
10 1/2	12 1/8	14	16 1/8	18 1 1/16	21 3/4	25 5/8	30 3/8	.....	0.230	
9 7/8	11 3/8	13 1/16	14 15/16	17 3/16	19 1 1/16	23	26 7/8	.....	0.240	
9 3/8	10 3/4	12 3/16	14	15 15/16	18 1/4	20 5/16	24 3/16	.....	0.250	
8 15/16	10 3/16	11 5/8	13 3/16	14 15/16	16 15/16	19 3/16	22 1/16	.....	0.260	
8 3/16	9 1 1/16	11	12 7/16	14 1/16	15 7/8	17 15/16	20 3/8	.....	0.270	
8 3/16	9 5/16	10 1/2	11 13/16	13 1/4	14 15/16	16 13/16	18 15/16	.....	0.280	
7 7/8	8 7/8	10 1/16	11 1/4	12 5/8	14 1/8	15 7/8	17 3/4	.....	0.290	
7 7/16	8 1/16	9 5/8	10 3/4	12	13 7/16	15	16 3/4	.....	0.300	
7 1/4	8 1/4	9 1/4	10 5/16	11 1/2	12 13/16	14 1/4	15 13/16	.....	0.310	
7	7 15/16	8 7/8	9 15/16	11 1/16	12 1/4	13 5/8	15 1/16	.....	0.320	
6 13/16	7 1 1/16	8 7/16	9 9/16	10 5/8	11 3/4	13	14 3/8	.....	0.330	
6 1/16	7 1/16	8 3/16	9 1/4	10 1/4	11 5/16	12 1/2	13 3/4	.....	0.340	
6 3/8	7 3/16	8	8 13/16	9 7/8	10 7/8	12	13 3/16	.....	0.350	
6 3/16	6 15/16	7 3/4	8 5/8	9 9/16	10 1/2	11 1/16	12 11/16	.....	0.360	
6	6 3/4	7 7/16	8 3/8	9 1/4	10 3/16	11 3/16	12 1/4	.....	0.370	
5 7/8	6 1/16	7 3/16	8 1/8	8 15/16	9 7/8	10 13/16	11 13/16	.....	0.380	
5 11/16	6 3/8	7 1/8	7 7/8	8 1 1/16	9 9/16	10 1/2	11 7/16	.....	0.390	
5 5/16	6 1/4	6 15/16	7 1 1/16	8 7/16	9 5/16	10 3/16	11 1/8	.....	0.400	
5 3/8	6 1/16	6 3/4	7 1/2	8 1/4	9	9 7/8	10 1/4	.....	0.410	
5 1/4	5 15/16	6 9/16	7 1/4	8	8 13/16	9 5/16	10 7/16	.....	0.420	
5 1/8	5 3/4	6 7/16	7 1/8	7 13/16	8 9/16	9 3/8	10 3/16	.....	0.430	
5	5 5/8	6 1/4	6 15/16	7 5/8	8 5/16	9 1/8	9 7/8	.....	0.440	
4 7/8	5 1/2	6 1/8	6 3/4	7 7/16	8 1/8	8 7/8	9 5/8	.....	0.450	
4 13/16	5 3/8	6	6 5/8	7 1/4	7 15/16	8 1 1/16	9 7/16	.....	0.460	
4 11/16	5 1/4	5 7/8	6 7/16	7 1/8	7 3/4	8 7/16	9 3/16	.....	0.470	
4 9/16	5 1/8	5 3/4	6 5/16	6 15/16	7 9/16	8 1/4	9	.....	0.480	
4 1/2	5 1/16	5 5/8	6 3/16	6 13/16	7 7/16	8 1/16	8 3/4	.....	0.490	
4 3/8	4 15/16	5 1/2	6 1/16	6 5/8	7 1/4	7 15/16	8 9/16	.....	0.500	
4 3/16	4 13/16	5 3/8	5 15/16	6 1/2	7 1/8	7 3/4	8 3/8	.....	0.510	
4 3/16	4 3/4	5 1/4	5 13/16	6 3/8	7	7 9/16	8 1/4	.....	0.520	
4 1/8	4 5/8	5 1/16	5 1 1/16	6 1/4	6 13/16	7 7/16	8 1/16	.....	0.530	



**TABLE 3-11 VALUES OF L FOR PIPE SIZES ≥ NPS 52 AND < NPS 56 (CONT'D)**

Depth, d, in.	Wall Thickness, t, in.							
	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.540	.....	.....	.....	.....	.....	.....	3/16	3/16
0.550	.....	.....	.....	.....	.....	.....	3	3/2
0.560	.....	.....	.....	.....	.....	.....	.....	3/8
0.570	.....	.....	.....	.....	.....	.....	.....	3/16
0.580	.....	.....	.....	.....	.....	.....	.....	3/4
0.590	.....	.....	.....	.....	.....	.....	.....	3/16
0.600	.....	.....	.....	.....	.....	.....	.....	3/8
0.610	.....	.....	.....	.....	.....	.....	.....	.....
0.620	.....	.....	.....	.....	.....	.....	.....	.....
0.630	.....	.....	.....	.....	.....	.....	.....	.....
0.640	.....	.....	.....	.....	.....	.....	.....	.....
0.650	.....	.....	.....	.....	.....	.....	.....	.....
0.660	.....	.....	.....	.....	.....	.....	.....	.....
0.670	.....	.....	.....	.....	.....	.....	.....	.....
0.680	.....	.....	.....	.....	.....	.....	.....	.....
0.690	.....	.....	.....	.....	.....	.....	.....	.....
0.700	.....	.....	.....	.....	.....	.....	.....	.....
0.710	.....	.....	.....	.....	.....	.....	.....	.....
0.720	.....	.....	.....	.....	.....	.....	.....	.....
0.730	.....	.....	.....	.....	.....	.....	.....	.....
0.740	.....	.....	.....	.....	.....	.....	.....	.....
0.750	.....	.....	.....	.....	.....	.....	.....	.....
0.760	.....	.....	.....	.....	.....	.....	.....	.....
0.770	.....	.....	.....	.....	.....	.....	.....	.....
0.780	.....	.....	.....	.....	.....	.....	.....	.....
0.790	.....	.....	.....	.....	.....	.....	.....	.....
0.800	.....	.....	.....	.....	.....	.....	.....	.....
0.810	.....	.....	.....	.....	.....	.....	.....	.....
0.820	.....	.....	.....	.....	.....	.....	.....	.....
0.830	.....	.....	.....	.....	.....	.....	.....	.....
0.840	.....	.....	.....	.....	.....	.....	.....	.....
0.850	.....	.....	.....	.....	.....	.....	.....	.....
0.860	.....	.....	.....	.....	.....	.....	.....	.....
0.870	.....	.....	.....	.....	.....	.....	.....	.....
0.880	.....	.....	.....	.....	.....	.....	.....	.....
0.890	.....	.....	.....	.....	.....	.....	.....	.....
0.900	.....	.....	.....	.....	.....	.....	.....	.....
0.910	.....	.....	.....	.....	.....	.....	.....	.....
0.920	.....	.....	.....	.....	.....	.....	.....	.....
0.930	.....	.....	.....	.....	.....	.....	.....	.....
0.940	.....	.....	.....	.....	.....	.....	.....	.....
0.950	.....	.....	.....	.....	.....	.....	.....	.....
0.960	.....	.....	.....	.....	.....	.....	.....	.....
0.970	.....	.....	.....	.....	.....	.....	.....	.....
0.980	.....	.....	.....	.....	.....	.....	.....	.....
0.990	.....	.....	.....	.....	.....	.....	.....	.....
1.000	.....	.....	.....	.....	.....	.....	.....	.....
1.010	.....	.....	.....	.....	.....	.....	.....	.....

**TABLE 3-11 VALUES OF L FOR PIPE SIZES ≥ NPS 52 AND < NPS 56 (CONT'D)**

0.812	0.875	0.938	Wall Thickness, t, in.					1.250	Depth, d, in.
			1.000	1.062	1.125	1.188	1.250		
4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>8</sub>	0.540	
3 <sup>15</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>3</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>4</sub>	0.550	
3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>16</sub>	7	7 <sup>5</sup> / <sub>8</sub>	0.560	
3 <sup>13</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>8</sub>	7 <sup>7</sup> / <sub>16</sub>	0.570	
3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>3</sup> / <sub>16</sub>	0.580	
3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>16</sub>	0.590	
3 <sup>5</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	5	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>9</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	0.600	
3 <sup>1</sup> / <sub>2</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>16</sub>	6 <sup>15</sup> / <sub>16</sub>	0.610	
3 <sup>7</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	0.620	
3 <sup>3</sup> / <sub>8</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	6 <sup>11</sup> / <sub>16</sub>	0.630	
3 <sup>5</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>8</sub>	0.640	
.....	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>1</sup> / <sub>2</sub>	0.650	
.....	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>8</sub>	0.660	
.....	3 <sup>3</sup> / <sub>16</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	0.670	
.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>7</sup> / <sub>16</sub>	0.680	
.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>8</sub>	0.690	
.....	3 <sup>3</sup> / <sub>8</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>9</sup> / <sub>16</sub>	6	0.700	
.....	.....	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	5	5 <sup>1</sup> / <sub>2</sub>	5 <sup>15</sup> / <sub>16</sub>	0.710	
.....	.....	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>13</sup> / <sub>16</sub>	0.720	
.....	.....	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	0.730	
.....	.....	3 <sup>7</sup> / <sub>16</sub>	4	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>11</sup> / <sub>16</sub>	0.740	
.....	.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	0.750	
.....	.....	.....	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>2</sub>	0.760	
.....	.....	.....	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5	5 <sup>7</sup> / <sub>16</sub>	0.770	
.....	.....	.....	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	0.780	
.....	.....	.....	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	0.790	
.....	.....	.....	3 <sup>5</sup> / <sub>8</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	0.800	
.....	.....	.....	.....	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>8</sub>	0.810	
.....	.....	.....	.....	3 <sup>7</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	0.820	
.....	.....	.....	.....	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>5</sup> / <sub>8</sub>	5	0.830	
.....	.....	.....	.....	3 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	0.840	
.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>7</sup> / <sub>8</sub>	0.850	
.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	0.860	
.....	.....	.....	.....	.....	4	4 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>	0.870	
.....	.....	.....	.....	.....	3 <sup>15</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	0.880	
.....	.....	.....	.....	.....	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>8</sub>	0.890	
.....	.....	.....	.....	.....	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	0.900	
.....	.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	0.910	
.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	0.920	
.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	0.930	
.....	.....	.....	.....	.....	.....	4	4 <sup>3</sup> / <sub>8</sub>	0.940	
.....	.....	.....	.....	.....	.....	3 <sup>15</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	0.950	
.....	.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>4</sub>	0.960	
.....	.....	.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>16</sub>	0.970	
.....	.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>8</sub>	0.980	
.....	.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>8</sub>	0.990	
.....	.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>16</sub>	1.000	
.....	.....	.....	.....	.....	.....	.....	.....	1.010	

**TABLE 3-12 VALUES OF L FOR PIPE SIZES ≥ NPS 56 AND < NPS 60**

Depth, d, in.	Wall Thickness, t, in.							
	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.040	.....	.....	.....	.....	.....	.....	.....	.....
0.050	21 <sup>3</sup> / <sub>16</sub>	22 <sup>3</sup> / <sub>16</sub>	22 <sup>5</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>16</sub>	.....	.....	.....	.....
0.060	21 <sup>3</sup> / <sub>16</sub>	22 <sup>3</sup> / <sub>16</sub>	22 <sup>5</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>16</sub>	25 <sup>1</sup> / <sub>16</sub>	.....	.....	.....
0.070	21 <sup>3</sup> / <sub>16</sub>	22 <sup>3</sup> / <sub>16</sub>	22 <sup>5</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>16</sub>	25 <sup>1</sup> / <sub>16</sub>	26 <sup>1</sup> / <sub>2</sub>	27 <sup>3</sup> / <sub>16</sub>	.....
0.080	14 <sup>3</sup> / <sub>16</sub>	19 <sup>1</sup> / <sub>16</sub>	22 <sup>5</sup> / <sub>16</sub>	23 <sup>1</sup> / <sub>16</sub>	25 <sup>1</sup> / <sub>16</sub>	26 <sup>1</sup> / <sub>2</sub>	27 <sup>3</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>
0.090	11 <sup>7</sup> / <sub>16</sub>	13 <sup>5</sup> / <sub>16</sub>	17 <sup>1</sup> / <sub>16</sub>	21 <sup>7</sup> / <sub>16</sub>	25 <sup>1</sup> / <sub>16</sub>	26 <sup>1</sup> / <sub>2</sub>	27 <sup>3</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>
0.100	9 <sup>1</sup> / <sub>2</sub>	11 <sup>1</sup> / <sub>2</sub>	13 <sup>5</sup> / <sub>16</sub>	15 <sup>7</sup> / <sub>16</sub>	23 <sup>5</sup> / <sub>16</sub>	26 <sup>1</sup> / <sub>2</sub>	27 <sup>3</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>
0.110	8 <sup>3</sup> / <sub>16</sub>	9 <sup>9</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>7</sup> / <sub>16</sub>	17 <sup>3</sup> / <sub>16</sub>	25 <sup>5</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>
0.120	7 <sup>1</sup> / <sub>4</sub>	8 <sup>3</sup> / <sub>8</sub>	9 <sup>9</sup> / <sub>16</sub>	11	14 <sup>1</sup> / <sub>2</sub>	19 <sup>1</sup> / <sub>16</sub>	27 <sup>3</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>
0.130	6 <sup>9</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>2</sub>	8 <sup>1</sup> / <sub>2</sub>	9 <sup>1</sup> / <sub>16</sub>	12 <sup>7</sup> / <sub>16</sub>	16 <sup>3</sup> / <sub>16</sub>	21 <sup>5</sup> / <sub>16</sub>	29 <sup>1</sup> / <sub>16</sub>
0.140	6	6 <sup>13</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	10 <sup>15</sup> / <sub>16</sub>	13 <sup>7</sup> / <sub>16</sub>	17 <sup>7</sup> / <sub>16</sub>	23 <sup>3</sup> / <sub>16</sub>
0.150	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	7 <sup>1</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	9 <sup>7</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>4</sub>	15 <sup>5</sup> / <sub>16</sub>	19 <sup>7</sup> / <sub>16</sub>
0.160	5 <sup>3</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>5</sup> / <sub>16</sub>	9	11 <sup>1</sup> / <sub>16</sub>	13 <sup>5</sup> / <sub>16</sub>	16 <sup>13</sup> / <sub>16</sub>
0.170	4 <sup>13</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	8 <sup>5</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>4</sub>	14 <sup>7</sup> / <sub>16</sub>
0.180	4 <sup>9</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	9 <sup>5</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>4</sub>	13 <sup>7</sup> / <sub>16</sub>
0.190	4 <sup>5</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>	8 <sup>1</sup> / <sub>16</sub>	10 <sup>3</sup> / <sub>8</sub>	12 <sup>3</sup> / <sub>16</sub>
0.200	4 <sup>1</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	11 <sup>3</sup> / <sub>8</sub>
0.210	3 <sup>7</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	10 <sup>5</sup> / <sub>16</sub>
0.220	3 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>5</sup> / <sub>16</sub>
0.230	3 <sup>1</sup> / <sub>2</sub>	3 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>7</sup> / <sub>16</sub>
0.240	3 <sup>3</sup> / <sub>8</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>9</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	8 <sup>15</sup> / <sub>16</sub>
0.250	3 <sup>1</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>8</sub>	4	4 <sup>7</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>8</sub>	8 <sup>1</sup> / <sub>2</sub>
0.260	3 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>2</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>8</sub>
0.270	2 <sup>15</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>3</sup> / <sub>4</sub>
0.280	2 <sup>7</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>7</sup> / <sub>16</sub>
0.290	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>4</sub>	7 <sup>3</sup> / <sub>16</sub>
0.300	2 <sup>5</sup> / <sub>8</sub>	3	3 <sup>5</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>16</sub>	6	6 <sup>7</sup> / <sub>8</sub>
0.310	2 <sup>9</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	5	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>8</sub>
0.320	2 <sup>7</sup> / <sub>16</sub>	2 <sup>3</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>16</sub>
0.330	.....	2 <sup>1</sup> / <sub>16</sub>	3	3 <sup>5</sup> / <sub>16</sub>	4	4 <sup>1</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>
0.340	.....	2 <sup>9</sup> / <sub>16</sub>	2 <sup>7</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>16</sub>
0.350	.....	2 <sup>1</sup> / <sub>2</sub>	2 <sup>13</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>7</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>
0.360	.....	.....	2 <sup>1</sup> / <sub>16</sub>	3	3 <sup>5</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>	5	5 <sup>1</sup> / <sub>16</sub>
0.370	.....	.....	2 <sup>5</sup> / <sub>8</sub>	2 <sup>15</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>2</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>
0.380	.....	.....	.....	2 <sup>13</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>
0.390	.....	.....	.....	2 <sup>3</sup> / <sub>4</sub>	3 <sup>5</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>
0.400	.....	.....	.....	2 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>4</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>
0.410	.....	.....	.....	.....	3 <sup>1</sup> / <sub>8</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>
0.420	.....	.....	.....	.....	3 <sup>5</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>13</sup> / <sub>16</sub>
0.430	.....	.....	.....	.....	3	3 <sup>9</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>
0.440	.....	.....	.....	.....	2 <sup>7</sup> / <sub>8</sub>	3 <sup>7</sup> / <sub>16</sub>	4	4 <sup>5</sup> / <sub>8</sub>
0.450	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>8</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>
0.460	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>4</sub>	3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>
0.470	.....	.....	.....	.....	.....	3 <sup>3</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>4</sub>	4 <sup>5</sup> / <sub>16</sub>
0.480	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>
0.490	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>	3 <sup>9</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>
0.500	.....	.....	.....	.....	.....	3	3 <sup>1</sup> / <sub>2</sub>	4
0.510	.....	.....	.....	.....	.....	.....	3 <sup>7</sup> / <sub>16</sub>	3 <sup>5</sup> / <sub>16</sub>
0.520	.....	.....	.....	.....	.....	.....	3 <sup>5</sup> / <sub>16</sub>	3 <sup>7</sup> / <sub>8</sub>
0.530	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>4</sub>	3 <sup>3</sup> / <sub>4</sub>

**TABLE 3-12 VALUES OF L FOR PIPE SIZES ≥ NPS 56 AND < NPS 60**

0.812	0.875	0.938	Wall Thickness, t, in.					Depth, d, in.
			1.000	1.062	1.125	1.188	1.250	
.....	.....	.....	.....	.....	.....	.....	.....	0.040
.....	.....	.....	.....	.....	.....	.....	.....	0.050
.....	.....	.....	.....	.....	.....	.....	.....	0.060
.....	.....	.....	.....	.....	.....	.....	.....	0.070
.....	.....	.....	.....	.....	.....	.....	.....	0.080
30 <sup>3</sup> / <sub>16</sub>	31 <sup>3</sup> / <sub>16</sub>	.....	.....	.....	.....	.....	.....	0.090
30 <sup>3</sup> / <sub>16</sub>	31 <sup>3</sup> / <sub>16</sub>	32 <sup>1</sup> / <sub>2</sub>	.....	.....	.....	.....	.....	0.100
30 <sup>3</sup> / <sub>16</sub>	31 <sup>3</sup> / <sub>16</sub>	32 <sup>1</sup> / <sub>2</sub>	33 <sup>1</sup> / <sub>2</sub>	34 <sup>3</sup> / <sub>16</sub>	.....	.....	.....	0.110
30 <sup>3</sup> / <sub>16</sub>	31 <sup>3</sup> / <sub>16</sub>	32 <sup>1</sup> / <sub>2</sub>	33 <sup>1</sup> / <sub>2</sub>	34 <sup>3</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	.....	0.120
30 <sup>3</sup> / <sub>16</sub>	31 <sup>3</sup> / <sub>16</sub>	32 <sup>1</sup> / <sub>2</sub>	33 <sup>1</sup> / <sub>2</sub>	34 <sup>3</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.130
30 <sup>3</sup> / <sub>16</sub>	31 <sup>3</sup> / <sub>16</sub>	32 <sup>1</sup> / <sub>2</sub>	33 <sup>1</sup> / <sub>2</sub>	34 <sup>3</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.140
25 <sup>1</sup> / <sub>4</sub>	31 <sup>3</sup> / <sub>16</sub>	32 <sup>1</sup> / <sub>2</sub>	33 <sup>1</sup> / <sub>2</sub>	34 <sup>3</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.150
21	26 <sup>15</sup> / <sub>16</sub>	32 <sup>1</sup> / <sub>2</sub>	33 <sup>1</sup> / <sub>2</sub>	34 <sup>3</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.160
18 <sup>3</sup> / <sub>16</sub>	22 <sup>9</sup> / <sub>16</sub>	28 <sup>11</sup> / <sub>16</sub>	33 <sup>1</sup> / <sub>2</sub>	34 <sup>3</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.170
16 <sup>3</sup> / <sub>16</sub>	19 <sup>5</sup> / <sub>16</sub>	24 <sup>3</sup> / <sub>16</sub>	30 <sup>3</sup> / <sub>16</sub>	34 <sup>3</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.180
14 <sup>5</sup> / <sub>16</sub>	17 <sup>1</sup> / <sub>2</sub>	21 <sup>1</sup> / <sub>16</sub>	25 <sup>11</sup> / <sub>16</sub>	31 <sup>7</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.190
13 <sup>3</sup> / <sub>16</sub>	15 <sup>13</sup> / <sub>16</sub>	18 <sup>13</sup> / <sub>16</sub>	22 <sup>7</sup> / <sub>16</sub>	27 <sup>7</sup> / <sub>16</sub>	33 <sup>3</sup> / <sub>16</sub>	36 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.200
12 <sup>3</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>2</sub>	17 <sup>1</sup> / <sub>16</sub>	20 <sup>1</sup> / <sub>16</sub>	23 <sup>3</sup> / <sub>4</sub>	28 <sup>5</sup> / <sub>16</sub>	35 <sup>3</sup> / <sub>16</sub>	37 <sup>1</sup> / <sub>2</sub>	0.210
11 <sup>1</sup> / <sub>16</sub>	13 <sup>3</sup> / <sub>16</sub>	15 <sup>5</sup> / <sub>16</sub>	18 <sup>3</sup> / <sub>16</sub>	21 <sup>1</sup> / <sub>16</sub>	25 <sup>3</sup> / <sub>16</sub>	30 <sup>7</sup> / <sub>16</sub>	36 <sup>5</sup> / <sub>16</sub>	0.220
10 <sup>7</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>16</sub>	14 <sup>1</sup> / <sub>2</sub>	16 <sup>3</sup> / <sub>4</sub>	19 <sup>5</sup> / <sub>16</sub>	22 <sup>3</sup> / <sub>16</sub>	26 <sup>3</sup> / <sub>16</sub>	31 <sup>3</sup> / <sub>16</sub>	0.230
10 <sup>1</sup> / <sub>4</sub>	11 <sup>13</sup> / <sub>16</sub>	13 <sup>3</sup> / <sub>16</sub>	15 <sup>1</sup> / <sub>2</sub>	17 <sup>13</sup> / <sub>16</sub>	20 <sup>9</sup> / <sub>16</sub>	23 <sup>7</sup> / <sub>16</sub>	27 <sup>7</sup> / <sub>16</sub>	0.240
9 <sup>3</sup> / <sub>4</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>4</sub>	14 <sup>1</sup> / <sub>2</sub>	16 <sup>3</sup> / <sub>16</sub>	18 <sup>13</sup> / <sub>16</sub>	21 <sup>3</sup> / <sub>4</sub>	25 <sup>1</sup> / <sub>16</sub>	0.250
9 <sup>1</sup> / <sub>4</sub>	10 <sup>9</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>16</sub>	13 <sup>11</sup> / <sub>16</sub>	15 <sup>1</sup> / <sub>2</sub>	17 <sup>5</sup> / <sub>16</sub>	20 <sup>1</sup> / <sub>16</sub>	22 <sup>7</sup> / <sub>16</sub>	0.260
8 <sup>7</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>16</sub>	12 <sup>13</sup> / <sub>16</sub>	14 <sup>3</sup> / <sub>16</sub>	16 <sup>1</sup> / <sub>2</sub>	18 <sup>5</sup> / <sub>16</sub>	21 <sup>1</sup> / <sub>16</sub>	0.270
8 <sup>1</sup> / <sub>2</sub>	9 <sup>5</sup> / <sub>16</sub>	10 <sup>7</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>4</sub>	13 <sup>3</sup> / <sub>4</sub>	15 <sup>1</sup> / <sub>2</sub>	17 <sup>1</sup> / <sub>16</sub>	19 <sup>5</sup> / <sub>16</sub>	0.280
8 <sup>1</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>	10 <sup>7</sup> / <sub>16</sub>	11 <sup>11</sup> / <sub>16</sub>	13 <sup>1</sup> / <sub>16</sub>	14 <sup>11</sup> / <sub>16</sub>	16 <sup>7</sup> / <sub>16</sub>	18 <sup>3</sup> / <sub>16</sub>	0.290
7 <sup>13</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	10	11 <sup>3</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>2</sub>	13 <sup>13</sup> / <sub>16</sub>	15 <sup>5</sup> / <sub>16</sub>	17 <sup>3</sup> / <sub>16</sub>	0.300
7 <sup>7</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>9</sup> / <sub>16</sub>	10 <sup>11</sup> / <sub>16</sub>	11 <sup>15</sup> / <sub>16</sub>	13 <sup>5</sup> / <sub>16</sub>	14 <sup>13</sup> / <sub>16</sub>	16 <sup>7</sup> / <sub>16</sub>	0.310
7 <sup>3</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>4</sub>	9 <sup>1</sup> / <sub>4</sub>	10 <sup>9</sup> / <sub>16</sub>	11 <sup>7</sup> / <sub>16</sub>	12 <sup>3</sup> / <sub>4</sub>	14 <sup>5</sup> / <sub>16</sub>	15 <sup>5</sup> / <sub>16</sub>	0.320
7 <sup>1</sup> / <sub>16</sub>	7 <sup>15</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	9 <sup>15</sup> / <sub>16</sub>	11	12 <sup>3</sup> / <sub>16</sub>	13 <sup>1</sup> / <sub>2</sub>	14 <sup>15</sup> / <sub>16</sub>	0.330
6 <sup>13</sup> / <sub>16</sub>	7 <sup>11</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>9</sup> / <sub>16</sub>	10 <sup>5</sup> / <sub>16</sub>	11 <sup>3</sup> / <sub>4</sub>	12 <sup>15</sup> / <sub>16</sub>	14 <sup>5</sup> / <sub>16</sub>	0.340
6 <sup>5</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>4</sub>	10 <sup>1</sup> / <sub>4</sub>	11 <sup>5</sup> / <sub>16</sub>	12 <sup>1</sup> / <sub>2</sub>	13 <sup>11</sup> / <sub>16</sub>	0.350
6 <sup>7</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>	8 <sup>1</sup> / <sub>16</sub>	8 <sup>15</sup> / <sub>16</sub>	9 <sup>7</sup> / <sub>16</sub>	10 <sup>15</sup> / <sub>16</sub>	12	13 <sup>3</sup> / <sub>16</sub>	0.360
6 <sup>1</sup> / <sub>4</sub>	7	7 <sup>3</sup> / <sub>16</sub>	8 <sup>11</sup> / <sub>16</sub>	9 <sup>9</sup> / <sub>16</sub>	10 <sup>9</sup> / <sub>16</sub>	11 <sup>5</sup> / <sub>16</sub>	12 <sup>11</sup> / <sub>16</sub>	0.370
6 <sup>1</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>5</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>4</sub>	11 <sup>1</sup> / <sub>4</sub>	12 <sup>5</sup> / <sub>16</sub>	0.380
5 <sup>15</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>	9	9 <sup>15</sup> / <sub>16</sub>	10 <sup>7</sup> / <sub>16</sub>	11 <sup>7</sup> / <sub>16</sub>	0.390
5 <sup>3</sup> / <sub>4</sub>	6 <sup>7</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	7 <sup>15</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>4</sub>	9 <sup>5</sup> / <sub>16</sub>	10 <sup>9</sup> / <sub>16</sub>	11 <sup>1</sup> / <sub>2</sub>	0.400
5 <sup>5</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7	7 <sup>3</sup> / <sub>4</sub>	8 <sup>1</sup> / <sub>2</sub>	9 <sup>3</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>4</sub>	11 <sup>3</sup> / <sub>16</sub>	0.410
5 <sup>7</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>9</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	9 <sup>15</sup> / <sub>16</sub>	10 <sup>7</sup> / <sub>16</sub>	0.420
5 <sup>1</sup> / <sub>16</sub>	6	6 <sup>1</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	9 <sup>1</sup> / <sub>16</sub>	10 <sup>9</sup> / <sub>16</sub>	0.430
5 <sup>3</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>3</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>7</sup> / <sub>16</sub>	10 <sup>1</sup> / <sub>4</sub>	0.440
5 <sup>1</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	7	7 <sup>11</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	9 <sup>3</sup> / <sub>16</sub>	10	0.450
5	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	7 <sup>9</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>4</sub>	9	9 <sup>3</sup> / <sub>4</sub>	0.460
4 <sup>7</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>5</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>	8 <sup>13</sup> / <sub>16</sub>	9 <sup>9</sup> / <sub>16</sub>	0.470
4 <sup>3</sup> / <sub>4</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	9 <sup>5</sup> / <sub>16</sub>	0.480
4 <sup>5</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	7 <sup>11</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>16</sub>	9 <sup>5</sup> / <sub>16</sub>	0.490
4 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	7 <sup>9</sup> / <sub>16</sub>	3 <sup>3</sup> / <sub>16</sub>	8 <sup>7</sup> / <sub>16</sub>	0.500
4 <sup>1</sup> / <sub>16</sub>	5	5 <sup>9</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>3</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	8 <sup>11</sup> / <sub>16</sub>	0.510
4 <sup>3</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>4</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>5</sup> / <sub>16</sub>	0.520
4 <sup>1</sup> / <sub>4</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>2</sub>	7 <sup>1</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>4</sub>	8 <sup>3</sup> / <sub>16</sub>	0.530



**TABLE 3-12 VALUES OF L FOR PIPE SIZES ≥ NPS 56 AND < NPS 60 (CONT'D)**

Depth, d, in.	Wall Thickness, t, in.							
	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750
0.540	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>
0.550	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>	3 <sup>1</sup> / <sub>16</sub>
0.560	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.570	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.580	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.590	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>16</sub>
0.600	.....	.....	.....	.....	.....	.....	.....	3 <sup>1</sup> / <sub>4</sub>
0.610	.....	.....	.....	.....	.....	.....	.....	.....
0.620	.....	.....	.....	.....	.....	.....	.....	.....
0.630	.....	.....	.....	.....	.....	.....	.....	.....
0.640	.....	.....	.....	.....	.....	.....	.....	.....
0.650	.....	.....	.....	.....	.....	.....	.....	.....
0.660	.....	.....	.....	.....	.....	.....	.....	.....
0.670	.....	.....	.....	.....	.....	.....	.....	.....
0.680	.....	.....	.....	.....	.....	.....	.....	.....
0.690	.....	.....	.....	.....	.....	.....	.....	.....
0.700	.....	.....	.....	.....	.....	.....	.....	.....
0.710	.....	.....	.....	.....	.....	.....	.....	.....
0.720	.....	.....	.....	.....	.....	.....	.....	.....
0.730	.....	.....	.....	.....	.....	.....	.....	.....
0.740	.....	.....	.....	.....	.....	.....	.....	.....
0.750	.....	.....	.....	.....	.....	.....	.....	.....
0.760	.....	.....	.....	.....	.....	.....	.....	.....
0.770	.....	.....	.....	.....	.....	.....	.....	.....
0.780	.....	.....	.....	.....	.....	.....	.....	.....
0.790	.....	.....	.....	.....	.....	.....	.....	.....
0.800	.....	.....	.....	.....	.....	.....	.....	.....
0.810	.....	.....	.....	.....	.....	.....	.....	.....
0.820	.....	.....	.....	.....	.....	.....	.....	.....
0.830	.....	.....	.....	.....	.....	.....	.....	.....
0.840	.....	.....	.....	.....	.....	.....	.....	.....
0.850	.....	.....	.....	.....	.....	.....	.....	.....
0.860	.....	.....	.....	.....	.....	.....	.....	.....
0.870	.....	.....	.....	.....	.....	.....	.....	.....
0.880	.....	.....	.....	.....	.....	.....	.....	.....
0.890	.....	.....	.....	.....	.....	.....	.....	.....
0.900	.....	.....	.....	.....	.....	.....	.....	.....
0.910	.....	.....	.....	.....	.....	.....	.....	.....
0.920	.....	.....	.....	.....	.....	.....	.....	.....
0.930	.....	.....	.....	.....	.....	.....	.....	.....
0.940	.....	.....	.....	.....	.....	.....	.....	.....
0.950	.....	.....	.....	.....	.....	.....	.....	.....
0.960	.....	.....	.....	.....	.....	.....	.....	.....
0.970	.....	.....	.....	.....	.....	.....	.....	.....
0.980	.....	.....	.....	.....	.....	.....	.....	.....
0.990	.....	.....	.....	.....	.....	.....	.....	.....
1.000	.....	.....	.....	.....	.....	.....	.....	.....
1.010	.....	.....	.....	.....	.....	.....	.....	.....

**TABLE 3-12 VALUES OF L FOR PIPE SIZES ≥ NPS 58 AND < NPS 60 (CONT'D)**

0.812	0.875	0.938	Wall Thickness, t, in.					Depth, d, in.
			1.000	1.062	1.125	1.188	1.250	
4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>8</sub>	6 <sup>15</sup> / <sub>16</sub>	7 <sup>9</sup> / <sub>16</sub>	8 <sup>3</sup> / <sub>16</sub>	0.540
4 <sup>1</sup> / <sub>2</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>13</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>16</sub>	0.550
4	4 <sup>9</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>5</sup> / <sub>16</sub>	7 <sup>7</sup> / <sub>8</sub>	0.560
3 <sup>15</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>9</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>8</sub>	7 <sup>3</sup> / <sub>4</sub>	0.570
3 <sup>7</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	7	7 <sup>5</sup> / <sub>8</sub>	0.580
3 <sup>13</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>3</sup> / <sub>8</sub>	6 <sup>7</sup> / <sub>8</sub>	7 <sup>7</sup> / <sub>16</sub>	0.590
3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>4</sub>	7 <sup>5</sup> / <sub>16</sub>	0.600
3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>11</sup> / <sub>16</sub>	7 <sup>3</sup> / <sub>16</sub>	0.610
3 <sup>9</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>1</sup> / <sub>2</sub>	6	6 <sup>9</sup> / <sub>16</sub>	7 <sup>1</sup> / <sub>16</sub>	0.620
3 <sup>1</sup> / <sub>2</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>7</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	7	0.630
3 <sup>7</sup> / <sub>16</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>13</sup> / <sub>16</sub>	6 <sup>5</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>8</sub>	0.640
.....	3 <sup>13</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>4</sub>	6 <sup>3</sup> / <sub>4</sub>	0.650
.....	3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>8</sub>	0.660
.....	3 <sup>11</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>9</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>16</sub>	6 <sup>9</sup> / <sub>16</sub>	0.670
.....	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>7</sup> / <sub>16</sub>	5 <sup>15</sup> / <sub>16</sub>	6 <sup>7</sup> / <sub>16</sub>	0.680
.....	3 <sup>9</sup> / <sub>16</sub>	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>7</sup> / <sub>8</sub>	6 <sup>5</sup> / <sub>16</sub>	0.690
.....	3 <sup>1</sup> / <sub>2</sub>	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	6 <sup>1</sup> / <sub>4</sub>	0.700
.....	.....	3 <sup>7</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>4</sub>	5 <sup>11</sup> / <sub>16</sub>	6 <sup>1</sup> / <sub>8</sub>	0.710
.....	.....	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>16</sub>	0.720
.....	.....	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	6	0.730
.....	.....	3 <sup>11</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>7</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	0.740
.....	.....	3 <sup>5</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	5 <sup>13</sup> / <sub>16</sub>	0.750
.....	.....	.....	4	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>5</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>4</sub>	0.760
.....	.....	.....	3 <sup>15</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>3</sup> / <sub>16</sub>	5 <sup>5</sup> / <sub>8</sub>	0.770
.....	.....	.....	3 <sup>7</sup> / <sub>8</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	5 <sup>9</sup> / <sub>16</sub>	0.780
.....	.....	.....	3 <sup>13</sup> / <sub>16</sub>	4 <sup>1</sup> / <sub>4</sub>	4 <sup>5</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>2</sub>	0.790
.....	.....	.....	3 <sup>3</sup> / <sub>4</sub>	4 <sup>3</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	5	5 <sup>7</sup> / <sub>16</sub>	0.800
.....	.....	.....	.....	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>15</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>8</sub>	0.810
.....	.....	.....	.....	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>8</sub>	5 <sup>1</sup> / <sub>4</sub>	0.820
.....	.....	.....	.....	4	4 <sup>3</sup> / <sub>8</sub>	4 <sup>13</sup> / <sub>16</sub>	5 <sup>3</sup> / <sub>16</sub>	0.830
.....	.....	.....	.....	3 <sup>15</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>16</sub>	4 <sup>3</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>8</sub>	0.840
.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>4</sub>	4 <sup>11</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>16</sub>	0.850
.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>16</sub>	4 <sup>5</sup> / <sub>8</sub>	5	0.860
.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>8</sub>	4 <sup>9</sup> / <sub>16</sub>	4 <sup>15</sup> / <sub>16</sub>	0.870
.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	4 <sup>7</sup> / <sub>8</sub>	0.880
.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>16</sub>	4 <sup>7</sup> / <sub>16</sub>	4 <sup>13</sup> / <sub>16</sub>	0.890
.....	.....	.....	.....	.....	4	4 <sup>3</sup> / <sub>8</sub>	4 <sup>3</sup> / <sub>4</sub>	0.900
.....	.....	.....	.....	.....	.....	4 <sup>5</sup> / <sub>16</sub>	4 <sup>11</sup> / <sub>16</sub>	0.910
.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>4</sub>	4 <sup>5</sup> / <sub>8</sub>	0.920
.....	.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>16</sub>	4 <sup>9</sup> / <sub>16</sub>	0.930
.....	.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>8</sub>	4 <sup>1</sup> / <sub>2</sub>	0.940
.....	.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>8</sub>	4 <sup>7</sup> / <sub>16</sub>	0.950
.....	.....	.....	.....	.....	.....	.....	4 <sup>7</sup> / <sub>16</sub>	0.960
.....	.....	.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>8</sub>	0.970
.....	.....	.....	.....	.....	.....	.....	4 <sup>5</sup> / <sub>16</sub>	0.980
.....	.....	.....	.....	.....	.....	.....	4 <sup>1</sup> / <sub>4</sub>	0.990
.....	.....	.....	.....	.....	.....	.....	4 <sup>3</sup> / <sub>16</sub>	1.000
.....	.....	.....	.....	.....	.....	.....	.....	1.010

This page intentionally left blank.



## PART 4 EVALUATION OF MAOP IN CORRODED AREAS

### 4.1 COMPUTATION OF $A$

If the measured maximum depth of the corroded area is greater than 10% of the nominal wall thickness but less than 80% of the nominal wall thickness and the measured longitudinal extent of the corroded area is greater than the value determined by Eq. (2) of Part 2, calculate

$$A = 0.893 \left( \frac{L_m}{\sqrt{Dt}} \right)$$

where

$L_m$  = measured longitudinal extent of the corroded area, in.

$D$  = nominal outside diameter of the pipe, in.

$t$  = nominal wall thickness of the pipe, in. Additional wall thickness required for concurrent external loads shall not be included in the calculations.

### 4.2 COMPUTATION OF $P'$

(a) For Values of  $A$  Less Than or Equal to 4.0.  $A$  and  $d/t$  determine a unique point on Fig. 4-1 corresponding to an acceptable pressure level  $P'$ .  $P'$  is obtained by interpolation between the curves for  $P$ ,  $0.95P$ ,  $0.90P$ ,  $0.85P$ ,  $0.80P$ ,  $0.75P$ ,  $0.70P$ ,  $0.65P$ ,  $0.60P$ .

$d$  = measured maximum depth of corroded area, in.

$P'$  = the safe maximum pressure for the corroded area. Curves for various values of  $P'$  are given in Fig. 4-1 per

$$P' = 1.1P \left[ \frac{1 - \frac{2}{3} \left( \frac{d}{t} \right)}{1 - \frac{2}{3} \left( \frac{d}{t\sqrt{A^2 + 1}} \right)} \right]$$

except that  $P'$  may not exceed  $P$ .

$P$  = the greater of either the established MAOP or

$$P = 2St/DT$$

where

$S$  = specified minimum yield strength (SMYS), psi



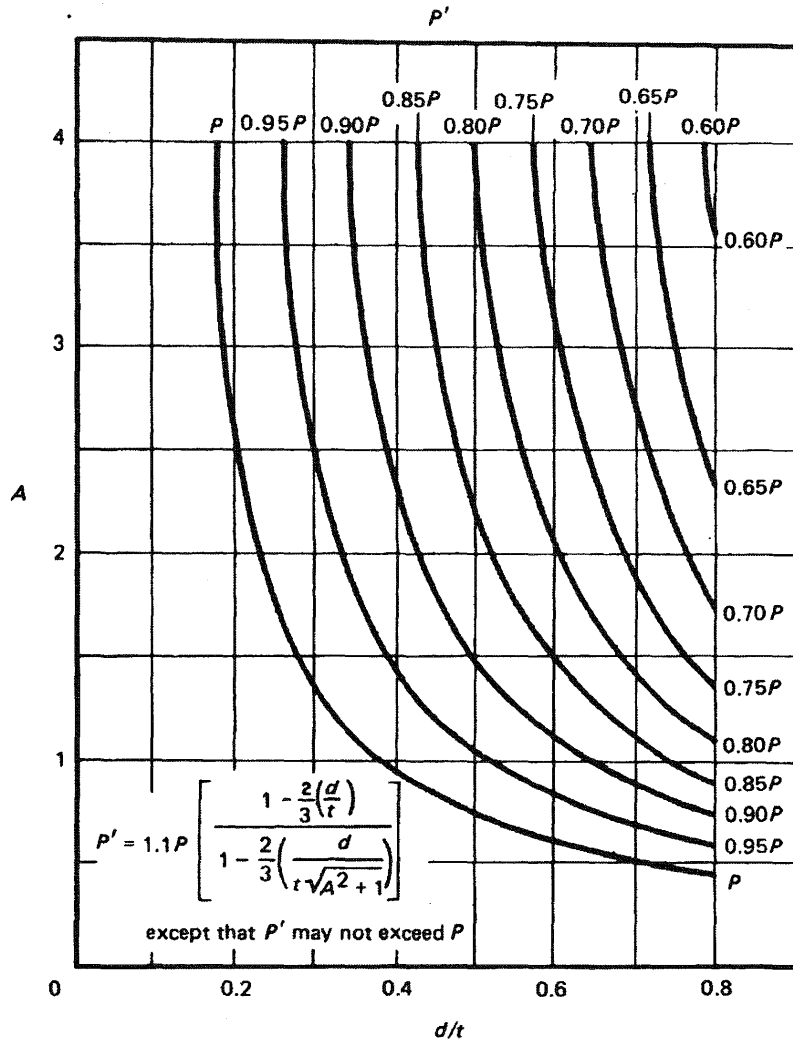


FIG. 4-1 CURVE FOR OBTAINING  $P'$  AS A FUNCTION OF  $d/t$  FOR VALUES OF  $A$  LESS THAN OR EQUAL TO 4.0

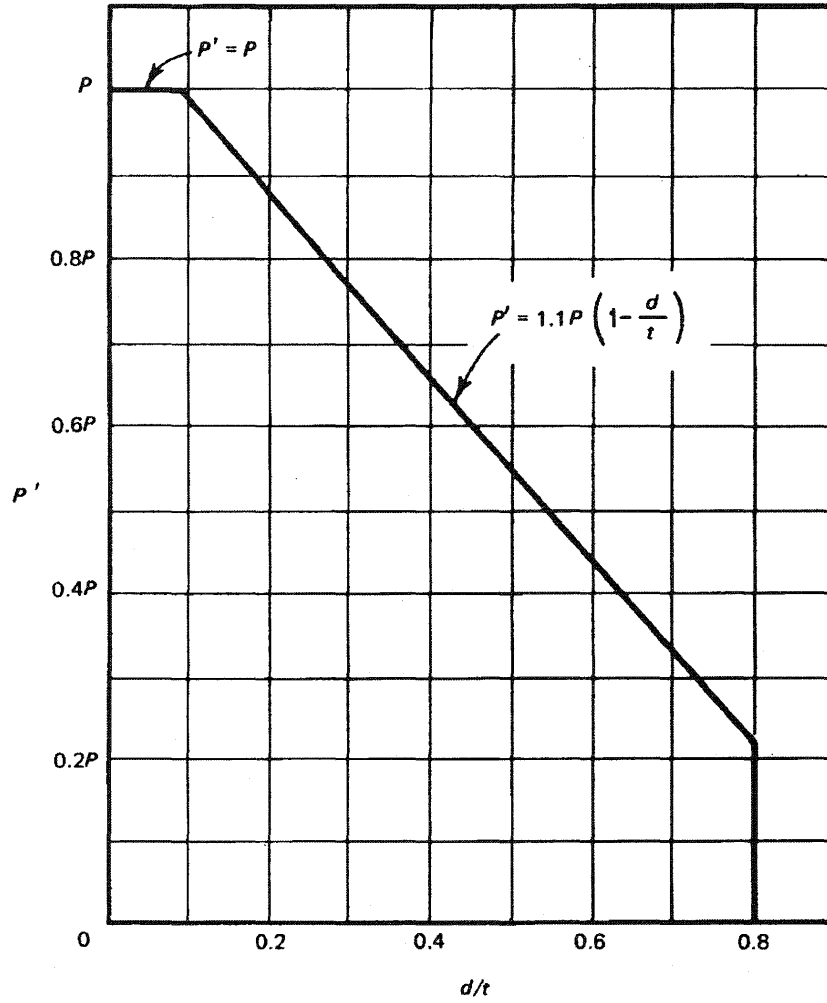


FIG. 4-2  $P'$  AS A FUNCTION OF  $d/t$  FOR VALUES OF A GREATER THAN 4.0

$F$  = appropriate design factor from ASME B31.4, ASME B31.8, or ASME B31.11

$T$  = temperature derating factor from the appropriate B31 Code (if none listed,  $T = 1$ )

$D$  = nominal outside diameter of the pipe, in.

$t$  = nominal wall thickness of the pipe, in. Additional wall thickness required for concurrent external loads shall not be included in the calculations.

(b) *For Values of A Greater Than 4.0*

$P'$  = the safe maximum pressure for the corroded area. Curves for various values of  $P'$  are given in Fig. 4-2 per

$$P' = 1.1P \left[ 1 - \frac{d}{t} \right]$$

except that  $P'$  may not exceed  $P$ .

### 4.3 MAOP AND $P'$

If the established MAOP is equal to or less than  $P'$ , the corroded region may be used for service at that MAOP. If it is greater than  $P'$ , then a lower MAOP should be established not to exceed  $P'$ , or the corroded region should be repaired or replaced.



**APPENDIX A**  
**BASIC Computer Program, CRVL.BAS,**  
**for Determining Allowable Length  $L$  (Part 2)**  
**or Alternative Maximum Allowable Operating Pressure (Part 4)**

Enter program and input as indicated. The examples should be used to verify correct entry of the program.





## PROGRAM LISTING FOR CRVL.BAS BY R.L.SEIFERT

```

10 'PROGRAM WRITTEN BY R.L.SEIFERT, TENNESSEE GAS PIPELINE COMPANY, IN MICROSOFT
    BASIC AND OPERABLE ON VARIOUS PERSONAL COMPUTERS, FEBRUARY 6, 1982, MODIFIED SEP
    TEMBER 1984.
20 'EVALUATE EXTERNALLY CORRODED HIGH PRESSURE GAS PIPING TO DETERMINE THE MAXIM
    UM PRESSURE THAT IT CAN SAFELY CONTAIN.
25 'THIS SYSTEM WAS DEVELOPED AT BATTELLE MEMORIAL INSTITUTE, COLUMBUS OHIO.
26 '***** PLEASE NOTE, THAT IF THE CORRODED SURFACE AREA EXTENDS ONTO OR ACROSS
    A WELD, THEN THIS METHOD IS NOT VALID. THE CORROSION MUST THEN BE EVALUATED BY
    COMPANY-DESIGNATED SPECIALISTS.*****
30 'COMPUTER WILL DISPLAY AN "ILLEGAL FUNCTION ERROR" IF MAOP IS SET HIGHER THAN
    1.1 X P, BECAUSE AN ATTEMPT TO FIND THE SQUARE ROOT OF A NEGATIVE NUMBER WILL R
    ESULT. IN PRACTICE, THE MAOP WOULD NEVER BE SET THAT HIGH.
40 ' IF MAOP IS SET SLIGHTLY BELOW 1.1 X P, AND CORROSION DEPTH IS ALMOST 10% OF
    WALL THICKNESS, COMPUTER MAY CALL FOR A REDUCTION OF PRESSURE, BUT IT WILL ALSO
    STATE THAT THERE IS NO RESTRICTION OF OPERATION DUE TO  $d < .1t$ .
50 'MAOP IS NEVER SET THAT HIGH IN PRACTICE, SO THIS SHOULD BE NO PROBLEM. THE
    10% ALLOWABLE DEPTH WITH NO OPERATING RESTRICTIONS SHOULD APPLY.
60 ' IF DEPTH OR LENGTH ARE SET TO ZERO, A RESPECTIVE SAFE LENGTH OR SAFE DEPTH W
    ILL BE DETERMINED, EVEN THOUGH THAT IS AN IMPOSSIBILITY. REGARD THE ZEROS AS IN
    FINITESIMALS RATHER THAN ZEROS. (0 = .000001, FOR EXAMPLE)
70 ' IF CORROSION DEPTH (d) IS ENTERED  $>1.5 \times$  WALL THICKNESS (t), THEN THE EXPRES
    SION  $(2/3 \times (t/d))$  WILL BE  $\geq 1$ . THIS WILL CAUSE A "DIVISION BY ZERO" ERROR IN TH
    E CALCULATIONS. DEPTH OF CORROSION CAN NEVER BE  $>$  WALL THICKNESS ANYWAY.
72 SCREEN 0,0,0:WIDTH 80:COLOR 14,1,0
75 DEFDBL A-Z
80 CLS:INPUT"MAXIMUM ALLOWABLE PRESSURE (MAOP) #/Sq.In.           ";M
90 INPUT"ENTER OUTSIDE DIAMETER OF PIPE (D) Inches             ";D
100 INPUT"ENTER PIPE WALL THICKNESS (t) Inch(es)              ";T
110 INPUT"ENTER STRENGTH OF STEEL (SMYS) Lbs/sq.in.           ";S
120 INPUT"ENTER DESIGN FACTOR (F) (.72,.60,.50,.40)           ";F
130 INPUT"ENTER MAXIMUM CORROSION DEPTH (d) Inch              ";DE
140 INPUT"MAX.LONGITDNAL.LGTH OF CORRODED AREA (L) Inches     ";L
150 PRINT:IF DE>.8*T THEN INPUT"DEPTH OF CORROSION EXCEEDS 80% OF PIPEWALL. PIPE
    MUST BE REPLACED.           PRESS <ENTER> FOR FURTHER EVALUATION.";EN
160 IF DE<=.1*T THEN INPUT"CORROSION DEPTH IS LESS THAN 10% OF PIPE WALL. NO RES
    TRICTIONS ON OPERATION.     PRESS <ENTER> FOR FURTHER EVALUATION.";EN
170 P=INT((2*S*T*F/D)+.5):A=(.893*L)/(D*T)^.5:A=(INT(1000*A))*0.001
180 IF A<=4 THEN PS=INT(1.1*P*((1-((2*DE)/(3*T)))/(1-((2/3)*(DE/(T*(A^2+1)^.5)))
    )+.5)
190 IF A>4 THEN PS=INT(1.1*P*(1-(DE/T))+.5)
195 IF PS>P THEN PS=P
200 CLS:PRINT           -- INPUTTED DATA --
210 PRINT"PIPE DIAMETER (D)=""D" In. ";TAB(30)"DESIGN FACTOR(F)=""F
220 PRINT"WALL THICKNESS(t)=""T" In. ";TAB(30)"MAX.COR.DPTH(d)=""DE" In.
230 PRINT"SMYS      ="S"PSI";TAB(30)"MAX.COR.LGTH(L)=""L" In.
240 PRINT"          MAOP=""M"PSI
250 PRINT"          -- CALCULATED DATA --
260 PRINT"          INTERMEDIATE FACTOR (A)= ";:PRINT USING "##.###";(INT(10
    00*A))*0.001
270 PRINT"DESIGN PRESS. (P)=""P"PSI";TAB(30)"SAFE PRESS. (P')=""PS"PSI"

** LISTING CONTINUES **

```



## PROGRAM LISTING FOR CRVL.BAS BY R.L.SEIFERT - CONTINUED

```

280 IF DE>.8*T THEN PRINT"REPAIR OR REPLACE PIPE BECAUSE CORROSION DEPTH EXCEEDS .8t."
290 IF PS=>M THEN PRINT"PIPE MAY BE OPERATED SAFELY AT MAOP,"M"PSI"
300 IF M>P THEN PRINT"MAOP EXCEEDS DESIGN PRESSURE (P). VERIFY THAT THIS VARIANCE IS VALID."
310 IF M>PS THEN PRINT"REDUCE OPERATING PRESSURE SO IT WILL NOT EXCEED"PS"PSI, SO THAT PIPE":PRINT"WILL OPERATE LEGALLY AND SAFELY."
330 IF A<4 THEN DP=((M-(1.1*P))*((3*T)*((A^2+1)^.5)))/(2*(M-((1.1*P)*((A^2+1)^.5)))):DP=(INT(1000*DP))*0.01
340 IF DP>.8*T THEN DF=.8*T
350 IF A<4 THEN PRINT"WITH CORR.LNGTH."L"In., MAX. DEPTH IS ";;PRINT USING "#.####";(INT((1000*DP)+.5))*0.01;PRINT" Inch. A = ";;PRINT USING "###.###";(INT((A*1000)+.5))*0.01
360 IF A>4 THEN DP=((M/(1.1*P))-1)*(-T)
370 IF DP>.8*T THEN DF=.8*T
380 IF A>4 THEN PRINT"WITH CORR.LNGTH."L"In., MAX.DEPTH IS ";;PRINT USING "#.####";(INT((1000*DP)+.5))*0.01;PRINT" Inch. A = ";;PRINT USING"###.###";(INT((A*1000)+.5))*0.01
390 AP=5:PS=INT(1.1*P*(1-(DE/T))+.5):IF PS>P THEN PS=P
400 IF M>PS THEN 420
410 PRINT"WITH CORR.DEPTH"DE"In., MAX. LENGTH IS INFINITY. A = ";;PRINT USING "###.###";AP:GOSUB 530:GOTO 470
420 J=(2*DE)/(3*T):AP=((J/(1-(((1.1*P)*(1-J))/M)))^2)-1)^.5:AP=INT((1000*AP)+.5)*.001:PS=INT(1.1*P*((1-J)/(1-((2/3)*(DE/(T*AP^2+1)^.5))))+.5):LP=INT((1000*((D*T)^.5)*1.12*AP)*.001:IF PS>P THEN PS=P
430 IF PS>M OR AP>4 THEN 450
440 PRINT"WITH CORR.DEPTH"DE"In., MAX. LENGTH IS ";;PRINT USING "###.###";INT(1000*((D*T)^.5)*1.12*AP)*.001;PRINT" In. A = ";;PRINT USING"###.###";(INT(AP*1000))*0.01:GOSUB 530:GOTO 470
450 AP=4:PS=1.1*P*((1-((2*DE)/(3*T)))/(1-((2/3)*(DE/(T*(AP^2+1)^.5))))):PS=INT(PS+.5):IF PS>P THEN PS=P
460 GOTO 440
470 PRINT:INPUT"PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE, OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.":
EN:IF EN<>1 THEN 20
480 CLS:PRINT"MAXIMUM ALLOWABLE OPERATING PRESSURE (MAOP) = "M"/sq.in.
490 PRINT"OUTSIDE DIAMETER OF PIPE (D) = "D" Inches
500 PRINT"PIPE WALL THICKNESS (t) = "T" Inch
510 PRINT"SPECIFIED MIN.YIELD STRENGTH OF PIPE (SMYS) = "S"/sq.in.
520 PRINT"DESIGN FACTOR (F) = "F:GOTO 130
530 IF DE>.8*T THEN PRINT"!!! BUT"DE" Inch EXCEEDS ALLOWABLE CORROSION DEPTH !!!"
540 RETURN

```

END OF PROGRAM LISTING



FOLLOWING ARE SOME EXAMPLES OF THE USE OF THE COMPUTER PROGRAM 'CRVL.BAS' BY R.L.SEIFERT, TENNESSEE GAS PIPELINE COMPANY.

THE PROGRAM PROMPTS THE USER ONE LINE AT A TIME FOR INPUT AS FOLLOWS:

EXAMPLE #1

```

MAXIMUM ALLOWABLE PRESSURE (MAOP) #/Sq.In.      ? 910
ENTER OUTSIDE DIAMETER OF PIPE (D) Inches      ? 30
ENTER PIPE WALL THICKNESS (t) Inch(es)         ? .438
ENTER STRENGTH OF STEEL (SMYS) Lbs/sq.in.     ? 52000
ENTER DESIGN FACTOR (F) (.72,.60,.50,.40)     ? .72
ENTER MAXIMUM CORROSION DEPTH (d) Inch        ? .1
MAX.LONGITDNAL.LGTH OF CORRODED AREA (L) Inches ? 7.5

```

AFTER THE USER HAS INPUTTED THE 7.5 IN THE LAST LINE (ABOVE), HE PRESSES THE <ENTER> KEY AND THE FOLLOWING READOUT RESULTS:

```

-- INPUTTED DATA --
PIPE DIAMETER (D)= 30 In.    DESIGN FACTOR(F)= .72
WALL THICKNESS(t) = .438 In. MAX.COR.DPTH(d) = .1 In.
SMYS      = 52000 PSI      MAOP = 910 PSI
-- CALCULATED DATA --
INTERMEDIATE FACTOR (A)= 1.847
DESIGN PRESS. (P)= 1093 PSI  SAFE PRESS. (P') = 1093 PSI
PIPE MAY BE OPERATED SAFELY AT MAOP, 910 PSI
WITH CORR.LNGTH. 7.5 In., MAX. DEPTH IS 0.2490 Inch.  A = 1.847
WITH CORR.DPTH .1 In., MAX. LENGTH IS INFINITY.  A = 5.000

```

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

FOLLOWING ARE MORE EXAMPLES OF PRINTOUTS OF VARIOUS CORROSION EVALUATIONS, SEVERAL OF WHICH REQUIRE REDUCTION OF PRESSURE, OR REPAIR, TO ALLOW RESUMPTION OF PIPELINE OPERATION.

EXAMPLE #2

```

-- INPUTTED DATA --
PIPE DIAMETER (D)= 20 In.    DESIGN FACTOR(F)= .5
WALL THICKNESS(t) = .25 In.  MAX.COR.DPTH(d) = .18 In.
SMYS      = 35000 PSI      MAOP = 400 PSI
-- CALCULATED DATA --
INTERMEDIATE FACTOR (A)= 3.993
DESIGN PRESS. (P)= 438 PSI  SAFE PRESS. (P') = 284 PSI
REDUCE OPERATING PRESSURE SO IT WILL NOT EXCEED 284 PSI, SO THAT PIPE
WILL OPERATE LEGALLY AND SAFELY.
WITH CORR.LNGTH. 10 In., MAX. DEPTH IS 0.0790 Inch.  A = 3.993
WITH CORR.DPTH .18 In., MAX. LENGTH IS 2.018 In.  A = 0.806

```

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?



EXAMPLE #3            -- INPUTTED DATA --  
 PIPE DIAMETER (D)= 24 In.    DESIGN FACTOR(F)= .72  
 WALL THICKNESS(t) = .432 In.    MAX.COR.DPTH(d) = .13 In.  
 SMYS        = 52000 PSI            MAX.COR.LGTH(L) = 30 In.  
    MAOP = 910 PSI  
    -- CALCULATED DATA --  
    INTERMEDIATE FACTOR (A)= 8.320  
 DESIGN PRESS.(P)= 1348 PSI    SAFE PRESS.(P') = 1037 PSI  
 PIPE MAY BE OPERATED SAFELY AT MAOP, 910 PSI  
 WITH CORR.LNGTH. 30 In., MAX.DEPTH IS 0.167 Inch.    A = 8.320  
 WITH CORR.DEPTH .13 In., MAX. LENGTH IS INFINITY.    A = 5.000

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
 OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

EXAMPLE #4            -- INPUTTED DATA --  
 PIPE DIAMETER (D)= 24 In.    DESIGN FACTOR(F)= .72  
 WALL THICKNESS(t) = .432 In.    MAX.COR.DPTH(d) = .3 In.  
 SMYS        = 52000 PSI            MAX.COR.LGTH(L) = 30 In.  
    MAOP = 910 PSI  
    -- CALCULATED DATA --  
    INTERMEDIATE FACTOR (A)= 8.320  
 DESIGN PRESS.(P)= 1348 PSI    SAFE PRESS.(P') = 453 PSI  
 REDUCE OPERATING PRESSURE SO IT WILL NOT EXCEED 453  
 PSI,                                    SO THAT PIPE WILL OPERATE LEGALLY AND SAFELY.  
 WITH CORR.LNGTH. 30 In., MAX.DEPTH IS 0.167 Inch.    A = 8.320  
 WITH CORR.DEPTH .3 In., MAX. LENGTH IS 12.867 In.    A = 3.568

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
 OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

EXAMPLE #5  
    -- INPUTTED DATA --  
 PIPE DIAMETER (D)= 24 In.    DESIGN FACTOR(F)= .72  
 WALL THICKNESS(t) = .281 In.    MAX.COR.DPTH(d) = .08 In.  
 SMYS        = 52000 PSI            MAX.COR.LGTH(L) = 15 In.  
    MAOP = 731 PSI  
    -- CALCULATED DATA --  
    INTERMEDIATE FACTOR (A)= 5.158  
 DESIGN PRESS.(P)= 877 PSI    SAFE PRESS.(P') = 690 PSI  
 REDUCE OPERATING PRESSURE SO IT WILL NOT EXCEED 690  
 PSI,                                    SO THAT PIPE WILL OPERATE LEGALLY AND SAFELY.  
 WITH CORR.LNGTH. 15 In., MAX.DEPTH IS 0.068 Inch.    A = 5.158  
 WITH CORR.DEPTH .08 In., MAX. LENGTH IS 11.634 In.    A = 4.000

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
 OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?



```

EXAMPLE #6
MAXIMUM ALLOWABLE PRESSURE (MAOP) #/Sq.In.           ? 1000
ENTER OUTSIDE DIAMETER OF PIPE (D) Inches           ? 36
ENTER PIPE WALL THICKNESS (t) Inch(es)              ? .5
ENTER STRENGTH OF STEEL (SMYS) Lbs/sq.in.          ? 52000
ENTER DESIGN FACTOR (F) (.72,.60,.50,.40)          ? .72
ENTER MAXIMUM CORROSION DEPTH (d) Inch              ? .41
MAX.LONGITDNAL.LGTH OF CORRODED AREA (L) Inches     ? 100

```

DEPTH OF CORROSION EXCEEDS 80% OF PIPEWALL. PIPE MUST BE REPLACED.  
PRESS <ENTER> FOR FURTHER EVALUATION.?

-- INPUTTED DATA --

```

PIPE DIAMETER (D)= 36 In.    DESIGN FACTOR(F)= .72
WALL THICKNESS(t) = .5 In.  MAX.COR.DPTH(d) = .41 In.
SMYS      = 52000 PSI        MAX.COR.LGTH(L) = 100 In.

```

MAOP = 1000 PSI

-- CALCULATED DATA --

```

INTERMEDIATE FACTOR (A)= 21.048
DESIGN PRESS.(P)= 1040 PSI  SAFE PRESS.(P') = 206 PSI
REPAIR OR REPLACE PIPE BECAUSE CORROSION DEPTH EXCEEDS .8t.
REDUCE OPERATING PRESSURE SO IT WILL NOT EXCEED 206 PSI, SO THAT PIPE
WILL OPERATE LEGALLY AND SAFELY.
WITH CORR.LNGTH. 100 In., MAX.DEPTH IS 0.0630 Inch.  A = 21.048
WITH CORR.DEPTH .41 In., MAX. LENGTH IS 2.556 In.  A = 0.538
!!! BUT .41 Inch EXCEEDS ALLOWABLE CORROSION DEPTH !!!

```

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

```

EXAMPLE #7
MAXIMUM ALLOWABLE PRESSURE (MAOP) #/Sq.In.           ? 877
ENTER OUTSIDE DIAMETER OF PIPE (D) Inches           ? 12.625
ENTER PIPE WALL THICKNESS (t) Inch(es)              ? .5
ENTER STRENGTH OF STEEL (SMYS) Lbs/sq.in.          ? 35000
ENTER DESIGN FACTOR (F) (.72,.60,.50,.40)          ? .4
ENTER MAXIMUM CORROSION DEPTH (d) Inch              ? .035
MAX.LONGITDNAL.LGTH OF CORRODED AREA (L) Inches     ? 3

```

CORROSION DEPTH IS LESS THAN 10% OF PIPE WALL. NO RESTRICTIONS ON OPERATION.  
PRESS <ENTER> FOR FURTHER EVALUATION.?

-- INPUTTED DATA --

```

PIPE DIAMETER (D)= 12.625 In. DESIGN FACTOR(F)= .4
WALL THICKNESS(t) = .5 In.    MAX.COR.DPTH(d) = .035 In.
SMYS      = 35000 PSI        MAX.COR.LGTH(L) = 3 In.

```

MAOP = 877 PSI

-- CALCULATED DATA --

```

INTERMEDIATE FACTOR (A)= 1.066
DESIGN PRESS.(P)= 1109 PSI  SAFE PRESS.(P') = 1109 PSI
PIPE MAY BE OPERATED SAFELY AT MAOP, 877 PSI
WITH CORR.LNGTH. 3 In., MAX. DEPTH IS 0.4000 Inch.  A = 1.066
WITH CORR.DEPTH .035 In., MAX. LENGTH IS INFINITY.  A = 5.000

```

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?



## EXAMPLE #8

```

-- INPUTTED DATA --
PIPE DIAMETER (D)= 24 In.    DESIGN FACTOR(F)= .5
WALL THICKNESS(t) = .5 In.  MAX.COR.DPTH(d) = .125 In.
SMYS      = 42000 PSI      MAX.COR.LGTH(L) = 12 In.
                          MAOP = 790 PSI
-- CALCULATED DATA --
INTERMEDIATE FACTOR (A)= 3.093
DESIGN PRESS.(P)= 875 PSI   SAFE PRESS.(P') = 845 PSI
PIPE MAY BE OPERATED SAFELY AT MAOP, 790 PSI
WITH CORR.LNGTH. 12 In., MAX. DEPTH IS 0.179 Inch. A = 3.093
WITH CORR.DEPTH .125 In., MAX. LENGTH IS 15.519 In. A = 4.000

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

```

THIS IS A TEST FOR THE ABOVE ALLOWABLE DEPTH AND LENGTH VALUES.  
TEST #1. ENTER DEPTH OF .179 AND LENGTH OF 12.

```

-- INPUTTED DATA --
PIPE DIAMETER (D)= 24 In.    DESIGN FACTOR(F)= .5
WALL THICKNESS(t) = .5 In.  MAX.COR.DPTH(d) = .179 In.
SMYS      = 42000 PSI      MAX.COR.LGTH(L) = 12 In.
                          MAOP = 790 PSI
-- CALCULATED DATA --
INTERMEDIATE FACTOR (A)= 3.093
DESIGN PRESS.(P)= 875 PSI   SAFE PRESS.(P') = 791 PSI
PIPE MAY BE OPERATED SAFELY AT MAOP, 790 PSI
WITH CORR.LNGTH. 12 In., MAX. DEPTH IS 0.179 Inch. A = 3.093
WITH CORR.DEPTH .179 In., MAX. LENGTH IS 12.182 In. A = 3.140

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

```

TEST #1A. ENTER DEPTH .179 AND LENGTH 12.182.

```

-- INPUTTED DATA --
PIPE DIAMETER (D)= 24 In.    DESIGN FACTOR(F)= .5
WALL THICKNESS(t) = .5 In.  MAX.COR.DPTH(d) = .179 In.
SMYS      = 42000 PSI      MAX.COR.LGTH(L) = 12.182 In.
                          MAOP = 790 PSI
-- CALCULATED DATA --
INTERMEDIATE FACTOR (A)= 3.140
DESIGN PRESS.(P)= 875 PSI   SAFE PRESS.(P') = 790 PSI
PIPE MAY BE OPERATED SAFELY AT MAOP, 790 PSI
WITH CORR.LNGTH. 12.182 In., MAX. DEPTH IS 0.178 Inch. A = 3.140
WITH CORR.DEPTH .179 In., MAX. LENGTH IS 12.182 In. A = 3.140

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

```



TEST #1B. INCREASING DEPTH BY A THOUSANDTH SHOULD CAUSE UNSAFE OPERATION.  
ENTER DEPTH OF .180 AND LENGTH OF 12.182

-- INPUTTED DATA --

PIPE DIAMETER (D) = 24 In. DESIGN FACTOR (F) = .5  
WALL THICKNESS (t) = .5 In. MAX. COR. DPTH (d) = .18 In.  
SMYS = 42000 PSI MAX. COR. LGTH (L) = 12.182 In.

MAOP = 790 PSI

-- CALCULATED DATA --

INTERMEDIATE FACTOR (A) = 3.140

DESIGN PRESS. (P) = 875 PSI SAFE PRESS. (P') = 789 PSI  
REDUCE OPERATING PRESSURE SO IT WILL NOT EXCEED 789  
PSI, SO THAT PIPE WILL OPERATE LEGALLY AND SAFELY.  
WITH CORR. LGTH. 12.182 In., MAX. DEPTH IS 0.178 Inch. A = 3.140  
WITH CORR. DEPTH .18 In., MAX. LENGTH IS 11.961 In. A = 3.083

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

TEST #2. INCREASING LENGTH BY A FEW HUNDREDTHS SHOULD CAUSE UNSAFE OPERATION.  
FROM THE SAFE CONDITION OF TEST #1A, INCREASE THE LENGTH FROM 12.182  
IN. TO 12.297 IN.

-- INPUTTED DATA --

PIPE DIAMETER (D) = 24 In. DESIGN FACTOR (F) = .5  
WALL THICKNESS (t) = .5 In. MAX. COR. DPTH (d) = .179 In.  
SMYS = 42000 PSI MAX. COR. LGTH (L) = 12.297 In.

MAOP = 790 PSI

-- CALCULATED DATA --

INTERMEDIATE FACTOR (A) = 3.170

DESIGN PRESS. (P) = 875 PSI SAFE PRESS. (P') = 789 PSI  
REDUCE OPERATING PRESSURE SO IT WILL NOT EXCEED 789  
PSI, SO THAT PIPE WILL OPERATE LEGALLY AND SAFELY.  
WITH CORR. LGTH. 12.297 In., MAX. DEPTH IS 0.1780 Inch. A = 3.170  
WITH CORR. DEPTH .179 In., MAX. LENGTH IS 12.182 In. A = 3.140

PRESS <1> FOR MORE CORROSION EVALUATIONS ON SAME PIPE,  
OR <2> FOR CORROSION EVALUATIONS ON DIFFERENT PIPE.?

\*\*\*\*\* END OF EXAMPLES \*\*\*\*\*

#### REFERENCES:

1. THE PROGRAMMABLE ELECTRONIC CALCULATOR IN UNDERGROUND CORROSION RELATED ACTIVITY. Part 2, "Determination of Safe Operating Pressure for a Corroded High Pressure Gas Pipeline" by R.L. Seifert. Materials Performance, Vol. 19, No. 7, (1980) July.
2. Kiefner, J.F., Duffy, A.R. Columbus Laboratories, Battelle Memorial Institute. SUMMARY OF RESEARCH TO DETERMINE THE STRENGTH OF CORRODED AREAS IN PIPE. (1971) 20 July
3. Marvin, C.W., DETERMINING THE STRENGTH OF CORRODED PIPE. Materials Protection and Performance, Vol. 11, No. 11, p. 34 (1972) November.
4. ASME GUIDE FOR GAS TRANSMISSION AND DISTRIBUTION PIPING SYSTEMS - 1976. Addendum No. 4, February, 1977 (Guide Material for Federal Standard 192.485), and Appendices G-6, G-7, and G-8.

=== END ===



**APPENDIX B**  
**BASIC Computer Program, CRLGTHU.BAS, Used in Generating**  
**Tables Like Those Which Are Printed in Part 3**

Following is the BASIC computer program CRLGTHU.BAS, whose forerunner, CRLGTH.BAS, was used for generating some of the tables in Part 3 with the same computer equipment that is used in Appendix A. This upgraded version, CRLGTHU.BAS, does not require the BASIC program to be modified with each use as did the former version, CRLGTH.BAS, which was included in earlier printing(s) of this manual.

Enter the BASIC program which is listed on the following pages into the computer, and check its operation by running it and entering the following data as prompted: pipe diameter = 20; shallowest pit depth = .03; wall thicknesses as follows: .406, .438, .469, .5, .562, .625, .688, .750, .812, and .875. The printout should duplicate the example which is printed at the end of this Appendix. (Printer commands in the program are for the Epson FX series and compatible printers, and could result in strange formats on other printers.)





## CRLGTHU.BAS

A computer program which provides the same type of information and printout as CRLGTH.BAS, except that the program does not need to be modified with each usage, and the user is asked for pipe diameter, the minimum pit depth to begin with, and up to 10 wall thicknesses. The program prompts the user for this information, in increasing order of thicknesses. (A thickness that is out of order will prompt a request to re-enter all of the thicknesses.)

```

10 'CRLGTHU.BAS
20 'THIS PROGRAM IS A UNIVERSAL PROGRAM, AND ALLOWS ENTRY OF ANY DIAMETER OF PIPE
   AND UP TO 10 WALL THICKNESSES TO EXAMINE FOR ALLOWABLE CORROSION LENGTHS.
30 CLS:'PROGRAM CRLGTHU.BAS BY R.L.SEIFERT TO LIST ALLOWED LENGTHS OF CORROSION
   FOR GIVEN DEPTHS OF CORROSION FOR SPECIFIED DIAMETER AND WALL THICKNESSES.FOR
   IBM-PC AND EPSON FX SERIES PRINTERS OR COMPATIBLE EQUIPMENT.
40 CLEAR 5000:DIM T(17):WIDTH "LPT1:",255
50 LPRINT CHR$(27);"@";:COLOR 7,1,0:CLS
60 PRINT TAB(30)"CRLGTHU.BAS"
70 PRINT TAB(26)"Revision of 2/17/89"
80 PRINT TAB(34)"by"
90 PRINT TAB(24)"Richard L. Seifert, P.E."
100 PRINT TAB(16)"Consultant for Pipeline Corrosion Control"
110 PRINT TAB(34)"and"
120 PRINT TAB(16)"Use and Application of Personal Computers"
130 PRINT TAB(25)"15602 Valley Bend Drive"
140 PRINT TAB(26)"Houston, Texas 77068"
150 PRINT
160 PRINT TAB(10)"This program prints a list of allowed lengths of corroded areas"
170 PRINT TAB(5)"on underground pressure piping for given pit depths. It is a
   general- "
180 PRINT TAB(5)"ized, conservative listing of allowed lengths, and if any
   corroded area "
190 PRINT TAB(5)"is 'condemned' by this listing, the corroded area should be
   examined
200 PRINT TAB(5)"further using Seifert's program CRVL.BAS. CRVL.BAS will examine
   the"
210 PRINT TAB(5)"corroded pipe using precise input parameters, and may allow the
   use of"
220 PRINT TAB(5)"the pipe, when this program, CRLGTHU.BAS, condemns it."

```



```

230 PRINT:PRINT TAB(22);:INPUT"Press <Enter> to proceed. ";EN
240 LPRINT CHR$(27);"@";:CLS:PRINT:INPUT"ADJUST PRINTER PAPER TO TOP OF FORM,
  TURN PRINTER ON, THEN PRESS <ENTER>";EN
250 INPUT"ENTER O.D. OF PIPE TO BE EXAMINED (EXAMPLE: 20)";D
260 INPUT"SHALLOWEST CORROSION DEPTH IN RANGE OF DEPTHS (E.G. .010)";DE:DE1=DE
270 J=0
280 PRINT"BEGIN ENTERING PIPE WALL THICKNESSES IN ASCENDING ORDER, FOR
  CALCULATIONS AND FOR COLUMN HEADINGS. MAXIMUM NUMBER OF ENTRIES = 10."
290 IF J=10 THEN J1=10:INPUT"MAXIMUM NUMBER OF THICKNESSES HAVE BEEN
  ENTERED. PRESS <ENTER> TO PROCEED.";EN:GOTO 330
300 J=J+1:PRINT"COLUMN "J". LAST ENTRY WAS "T(J-1):INPUT"ENTER WALL THICKNESS
  FOR THIS COLUMN. (-1 TO END ENTRIES) ";T(J)
310 IF T(J)=-1 THEN J=J-1:J1=J:GOTO 330
320 GOTO 290
330 FOR J=1 TO J1
340 IF T(J)<T(J-1) THEN BEEP:CLS:FOR Q=1 TO J1-1:PRINT T(Q) " ";:NEXT Q:PRINT
  T(J1):ELSE 360
350 PRINT:PRINT"Wall thicknesses are all not in ascending order. You must re-enter
  wall thicknesses. Press <Enter> for re-entry of wall
  thicknesses. ":INPUT;EN:CLS:GOTO 270
360 NEXT J
370 LPRINT CHR$(27)"0";:FOR N=1 TO 4:LPRINT:NEXT N:LPRINT CHR$(27)"U";CHR$(1);
380 LPRINT CHR$(27)"G";:LPRINT CHR$(18);TAB(17)"VALUES OF L FOR PIPE WITH
  O.D. OF"D"INCHES"
390 LPRINT STRING$(75,"*")
400 LPRINT CHR$(15);
410 LPRINT"Pit Depth";TAB(60)"Wall Thickness (t), Inches";TAB(128)"
420 J2=19:LPRINT"d(Inch) ";:LPRINT USING "##.###";T(1);:FOR J=2 TO J1:LPRINT
  TAB(J2) USING "##.###";T(J);:J2=J2+12:NEXT J:LPRINT TAB(128)"
430 LPRINT STRING$(127,"=");:"
440 FOR N=1 TO 150
450 TAB=0:IF INT(N/5)=N/5 THEN TAB=1:TAB2=1:LPRINT
  CHR$(27)CHR$(45)CHR$(1);:'START UNDERLINE
460 LPRINT USING"##.###";(INT((DE*1000)+.5))*0.001;:LPRINT"!";:TAB=TAB+19:IF
  DE=DE1 AND DE/T(1)<.1 THEN TAB=TAB-1
470 FOR J=1 TO J1
480 T=T(J)
490 IF DE/T<.1 OR DE/T>.8 THEN L$=" ":GOTO 620
500 IF 100*(DE/T)=>10 AND 100*(DE/T)=<17.5 THEN B=4:GOTO 520
510 B=SQR(((DE/T)/((1.1*(DE/T))-0.15))^2-1)
520 L=1.12*B*SQR(D*T)
530 L2=L-INT(L):L3=INT((L2/.0625)+.5):L4$=STR$(L3)+" /16":L=INT(L)
540 IF L3=0 THEN 560
550 IF 16/L3=2 THEN L4$=" 1/2":GOTO 600

```



```

560 IF L3=0 THEN L4$=" ":GOTO 600
570 IF L3=16 THEN L=L+1:L4$=" ":GOTO 600
580 IF INT(L3/2)=L3/2 THEN L3=L3/2:L4$=STR$(L3)+"/8"
590 IF INT(L3/2)≠L3/2 THEN L3=L3/2:L4$=STR$(L3)+"/4"
600 IF L=0 THEN L$=" "+L4$:ELSE L$=STR$(L)+L4$
610 IF LEN(STR$(L))=2 THEN LPRINT" ";
620 GOTO 630
630 LPRINT L$;:IF DE=DE1 THEN 640: ELSE LPRINT TAB(TAB);:TAB=TAB+12:GOTO 650
640 LPRINT TAB(TAB-1);:TAB=TAB+12
650 NEXT J
660 IF DE=DE1 THEN LPRINT TAB(128)"":ELSE LPRINT TAB(128+TAB2)" !"
670 LPRINT CHR$(27)CHR$(45)CHR$(0);:TAB2=0 'STOP UNDERLINE
680 IF DE>((T(J1)*.8)+.01) AND L$=" " THEN LPRINT:LPRINT:LPRINT:LPRINT
CHR$(27)"2":LPRINT CHR$(27)"U"CHR$(0);:LPRINT CHR$(27)"H";:WIDTH
"LPT1:",80:LPRINT CHR$(18);:GOTO 710
690 DE=DE+.01
700 NEXT N
710 FL=1:CLS:Y$="":PRINT:INPUT"Do you want to print another table of acceptable
corrosion lengths (Y/N*);Y$:IF Y$="n" OR Y$="N" OR Y$="" THEN END
720 CLEAR 5000:DIM T(17):WIDTH "LPT1:",255
730 LPRINT CHR$(27);"@";:COLOR 7,1,0:CLS:GOTO 240

```



VALUES OF L FOR PIPE WITH O.D. OF 20 INCHES										
Pit Depth d(Inch)	Wall Thickness (t), Inches									
	0.406	0.438	0.469	0.500	0.562	0.625	0.688	0.750	0.812	0.875
0.030										
0.040										
0.050	12 3/4	13 1/4	13 3/4							
0.060	12 3/4	13 1/4	13 3/4	14 3/16	15					
0.070	12 3/4	13 1/4	13 3/4	14 3/16	15	15 13/16	16 5/8			
0.080	8 7/8	11 7/16	13 3/4	14 3/16	15	15 13/16	16 5/8	17 3/8		
0.090	6 13/16	8 5/16	10 3/16	12 13/16	15	15 13/16	16 5/8	17 3/8	18 1/16	18 3/4
0.100	5 11/16	6 11/16	7 15/16	9 1/2	14 1/8	15 13/16	16 5/8	17 3/8	18 1/16	18 3/4
0.110	4 7/8	5 11/16	6 5/8	7 11/16	10 5/8	15 1/2	16 5/8	17 3/8	18 1/16	18 3/4
0.120	4 5/16	5	5 3/4	6 9/16	8 11/16	11 3/4	16 5/8	17 3/8	18 1/16	18 3/4
0.130	3 15/16	4 1/2	5 1/16	5 3/4	7 7/16	9 11/16	12 15/16	17 3/8	18 1/16	18 3/4
0.140	3 9/16	4 1/16	4 5/8	5 3/16	6 9/16	8 5/16	10 11/16	14	18 1/16	18 3/4
0.150	3 5/16	3 3/4	4 3/16	4 3/4	5 7/8	7 5/16	9 3/16	11 5/8	15	18 3/4
0.160	3 1/16	3 1/2	3 7/8	4 3/8	5 3/8	6 5/8	8 1/8	10 1/16	12 9/16	16 1/16
0.170	2 7/8	3 1/4	3 5/8	4 1/16	4 15/16	6 1/16	7 5/16	8 7/8	10 7/8	13 1/2
0.180	2 11/16	3 1/16	3 7/16	3 13/16	4 5/8	5 9/16	6 11/16	8 1/16	9 11/16	11 3/4
0.190	2 9/16	2 7/8	3 3/16	3 9/16	4 5/16	5 3/16	6 3/16	7 3/8	8 3/4	10 7/16
0.200	2 7/16	2 3/4	3 1/16	3 3/8	4 1/16	4 7/8	5 3/4	6 13/16	8	9 7/16
0.210	2 5/16	2 5/8	2 7/8	3 3/16	3 7/8	4 9/16	5 7/16	6 3/8	7 7/16	8 11/16
0.220	2 3/16	2 1/2	2 3/4	3 1/16	3 5/8	4 5/16	5 1/8	5 15/16	6 15/16	8 1/6
0.230	2 1/8	2 3/8	2 5/8	2 7/8	3 1/2	4 1/8	4 13/16	5 5/8	6 1/2	7 1/2
0.240	2	2 1/4	2 1/2	2 3/4	3 5/16	3 15/16	4 5/8	5 5/16	6 1/8	7 1/16
0.250	1 15/16	2 3/16	2 7/16	2 11/16	3 3/16	3 3/4	4 3/8	5 1/16	5 13/16	6 11/16
0.260	1 7/8	2 1/16	2 5/16	2 9/16	3 1/16	3 5/8	4 3/16	4 13/16	5 9/16	6 5/16
0.270	1 3/4	2	2 1/4	2 7/16	2 15/16	3 7/16	4	4 5/8	5 5/16	6
0.280	1 11/16	1 15/16	2 1/8	2 3/8	2 13/16	3 5/16	3 7/8	4 7/16	5 1/16	5 3/4
0.290	1 5/8	1 7/8	2 1/16	2 1/4	2 3/4	3 3/16	3 3/4	4 1/4	4 7/8	5 1/2
0.300	1 9/16	1 3/4	2	2 3/16	2 5/8	3 1/8	3 5/8	4 1/8	4 11/16	5 5/16
0.310	1 1/2	1 11/16	1 15/16	2 1/8	2 9/16	3	3 1/2	4	4 1/2	5 1/8
0.320	1 7/16	1 5/8	1 7/8	2 1/16	2 7/16	2 7/8	3 3/8	3 7/8	4 3/8	4 15/16
0.330		1 5/8	1 13/16	2	2 3/8	2 13/16	3 1/4	3 3/4	4 3/16	4 3/4
0.340		1 9/16	1 3/4	1 15/16	2 5/16	2 3/4	3 1/8	3 5/8	4 1/16	4 5/8
0.350		1 1/2	1 11/16	1 7/8	2 1/4	2 5/8	3 1/16	3 1/2	3 15/16	4 7/16
0.360			1 5/8	1 13/16	2 3/16	2 9/16	3	3 3/8	3 13/16	4 5/16
0.370			1 9/16	1 3/4	2 1/8	2 1/2	2 7/8	3 5/16	3 3/4	4 3/16
0.380				1 11/16	2 1/16	2 7/16	2 13/16	3 3/16	3 5/8	4 1/16
0.390				1 5/8	2	2 3/8	2 3/4	3 1/8	3 1/2	3 15/16
0.400				1 9/16	1 15/16	2 5/16	2 11/16	3 1/16	3 7/16	3 7/8
0.410					1 7/8	2 1/4	2 9/16	2 15/16	3 3/8	3 3/4
0.420					1 13/16	2 3/16	2 1/2	2 7/8	3 1/4	3 11/16
0.430					1 3/4	2 1/8	2 7/16	2 13/16	3 3/16	3 9/16
0.440					1 3/4	2 1/16	2 3/8	2 3/4	3 1/8	3 1/2
0.450						2	2 3/8	2 11/16	3 1/16	3 7/16
0.460						1 15/16	2 5/16	2 5/8	3	3 5/16
0.470						1 15/16	2 1/4	2 9/16	2 7/8	3 1/4
0.480						1 7/8	2 3/16	2 1/2	2 13/16	3 3/16
0.490						1 13/16	2 1/8	2 7/16	2 3/4	3 1/8
0.500						1 3/4	2 1/16	2 3/8	2 3/4	3 1/16
0.510							2 1/16	2 3/8	2 11/16	3
0.520							2	2 5/16	2 5/8	2 15/16
0.530							1 15/16	2 1/4	2 9/16	2 7/8
0.540							1 15/16	2 3/16	2 1/2	2 13/16
0.550							1 7/8	2 3/16	2 7/16	2 3/4
0.560							2 1/8	2 3/8	2 11/16	2 11/16
0.570							2 1/16	2 3/8	2 11/16	2 11/16
0.580								2	2 5/16	2 5/8
0.590								2	2 1/4	2 9/16
0.600								1 15/16	2 1/4	2 1/2
0.610									2 3/16	2 7/16
0.620									2 1/8	2 7/16
0.630									2 1/8	2 3/8
0.640									2 1/16	2 5/16
0.650										2 5/16
0.660										2 1/4
0.670										2 3/16
0.680										2 3/16
0.690										2 1/8
0.700										2 1/8
0.710										
0.720										

## ASME CODE FOR PRESSURE PIPING, B31

Power Piping .....	B31.1-1989
Chemical Plant and Petroleum Refinery Piping .....	B31.3-1990
Liquid Transportation Systems for Hydrocarbons, Liquid Petroleum Gas, Anhydrous Ammonia, and Alcohols .....	B31.4-1989
Refrigeration Piping .....	B31.5-1987
Gas Transmission and Distribution Piping Systems .....	B31.8-1989
Building Services Piping .....	B31.9-1988
Slurry Transportation Piping Systems .....	B31.11-1989
Manual for Determining the Remaining Strength of Corroded Pipelines: A Supplement to ASME B31 Code for Pressure Piping .....	B31G-1991

